



Applicazione di CNT in matrici elastomeriche

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Dipartimento di Chimica, Materiali, Ingegneria Chimica "G. Natta"

**Nanotubi di carbonio:
sintesi, applicazioni ed opportunità**

16 maggio 2013

Politecnico di Milano

Piazza Leonardo da Vinci 32, Aula Giulio Natta

Items of the presentation

- 👉 Processing methods for the preparation of nanocomposites
- 👉 CNT organization in the polymer matrix
 - distribution and dispersion
 - structure and aspect ratio
- 👉 CNT – polymer interface
- 👉 Properties of CNT based nanocomposites
 - vulcanization behaviour
 - electrical conductivity
 - thermal conductivity
 - mechanical reinforcement
- 👉 Hybrid filler systems based on CNT

Processing methods for the preparation of CNT based nanocomposites

Processing methods for the preparation of nanocomposites

☞ *Dry* melt blending

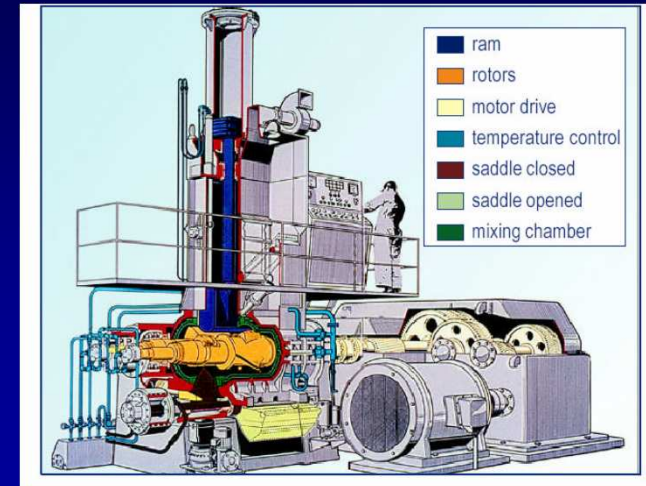
☞ *Wet* melt blending

☞ Solution blending

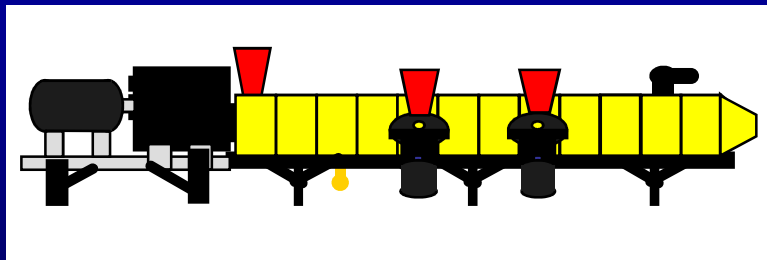
Melt blending



two roll mill



Banbury®



Twin screw extruder



Brabender®

Dry melt blending

PI introduced in the internal mixer and masticated
90 – 100°C, 1 min, rotors: 30 rpm

CNT added - mixing: 100°C, 4 min

Composite discharged

Addition of activators and curatives
mixing: 60°C, 4 min

Composite discharged

Composite homogeneized at two roll mill.
5 times, rotors: 38 and 30 rpm

Successive steps

Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
Macromol. Mater. Eng. 2012, 298(2), 241-251

Wet melt blending



CNT in EtOH = 1:10 wt + non-ionic surfactant

Ultrasonication: 200W_{effective}, 25kHz, 2h

S-SBR / BR = 50 / 50 on a two-roll mill and masticated

80°C , 5min

Addition of CNT / EtOH - mixing 15min

Composite discharged

Addition of activators and curatives at two roll mill:

mixing at RT

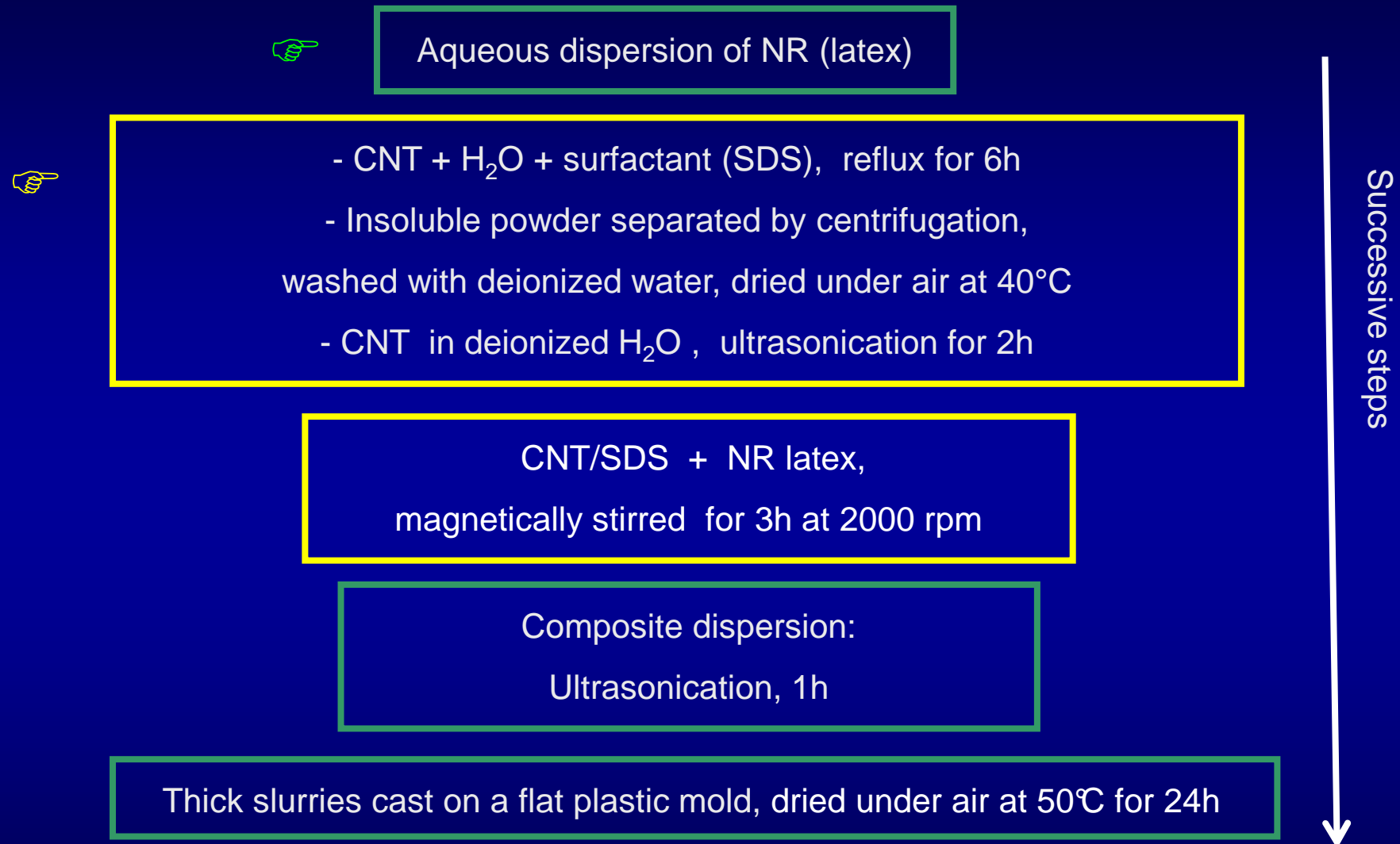
Composite homogeneized at two roll mill

25 min

Successive steps

A. Das, K.W. Stockelhuber, R. Jurk, M. Saphiannikova, J. Fritzsche, H. Lorenz, M. Kuppler, G. Heinrich
Polymer 2008, 49, 5276 - 5283

Latex blending



C. F. Matos, F. Galembeck, A. J. G. Zarbin
Carbon 2012, 50, 4685-4695

Solution blending



NR dissolved in toluene



CNT sonicated in toluene
30 min

Addition of CNT/toluene to NR/toluene:
mechanically stirred for 20min, then dried in open air at RT

Addition of activators and curatives
at two roll mill, 80°C, 15min

Successive steps

A.A. Abdullateef, S.P. Thomas, M. A. Al-Harhi, S.K. De, S. Bandyopadhyay, A.A. Basfar, M. A. Atieh;
Journal of Applied Polymer Science 2012, 125, E76 – E84

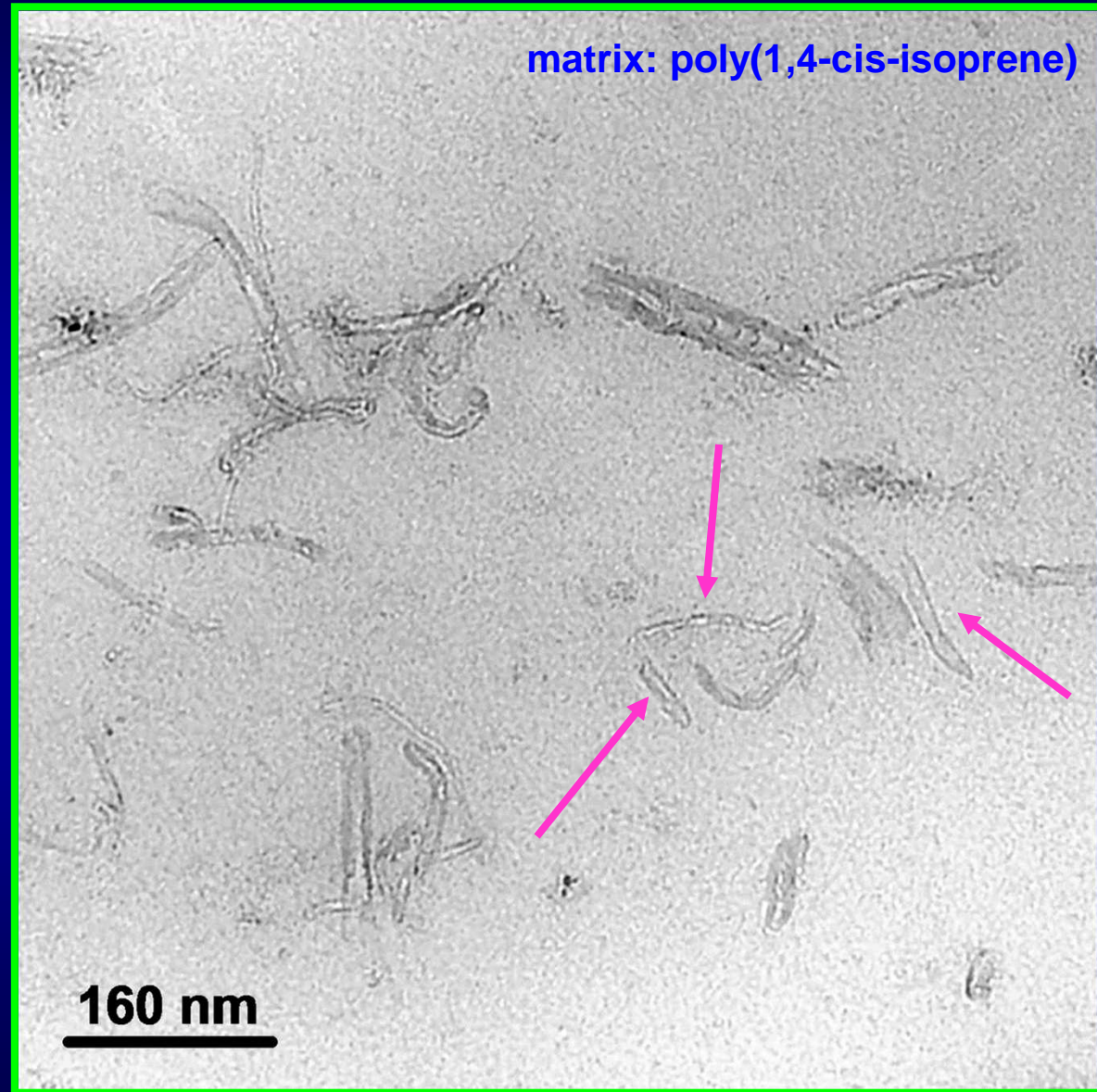
CNT organization in the polymer matrix

Composites from dry melt blending

IR	100
CNT	5

Well dispersed CNT

CNT broken
by mixing



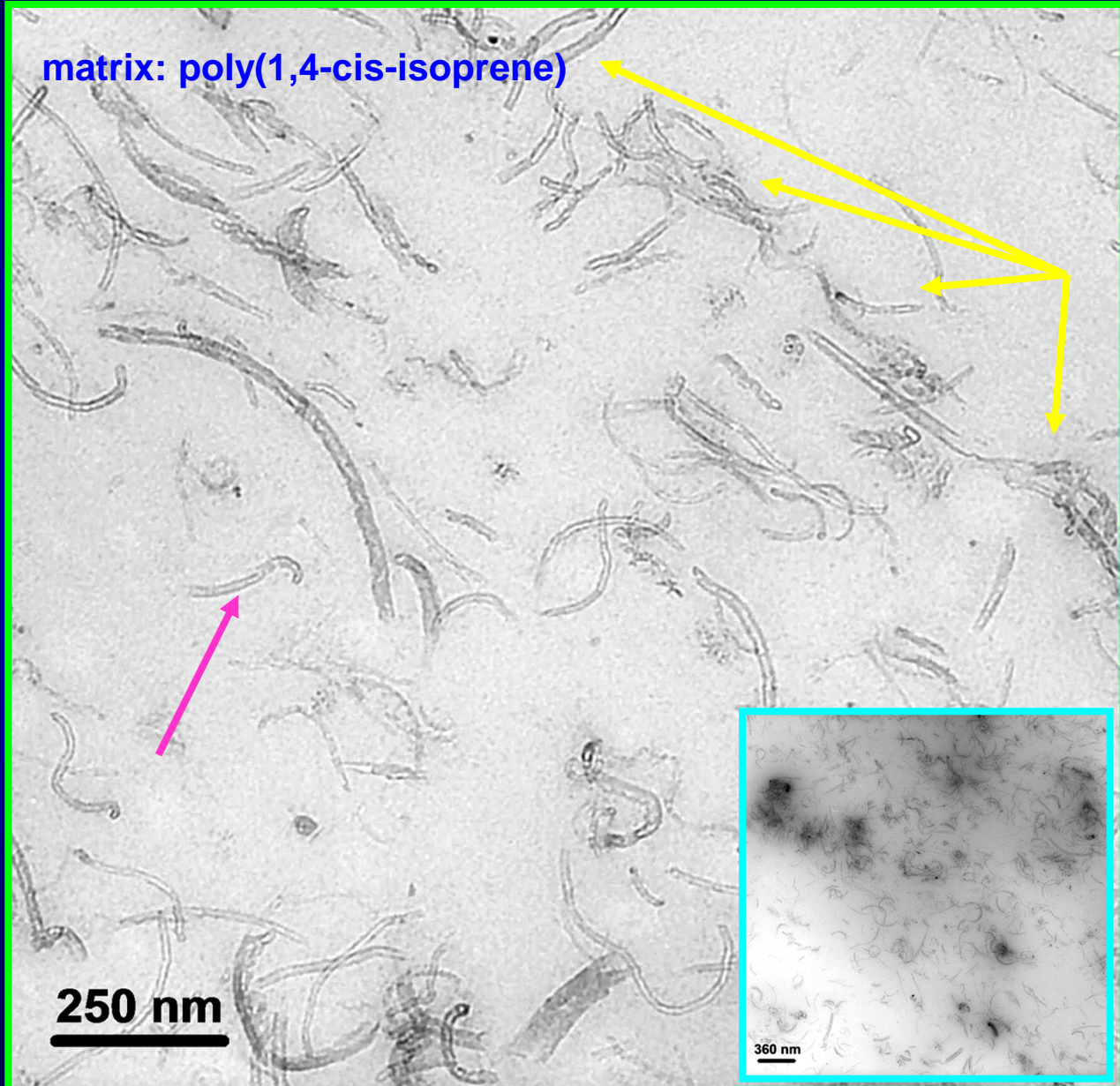
Galimberti M. et al
Macromol. Mater. Eng. 2012, 298(2), 241-251

Composites from dry melt blending

IR	100
CNT	11

CNT broken
by mixing

CNT percolation
at 7 phr



Galimberti M. et al
Macromol. Mater. Eng. 2012, 298(2), 241-251

Composites from *wet* melt blending

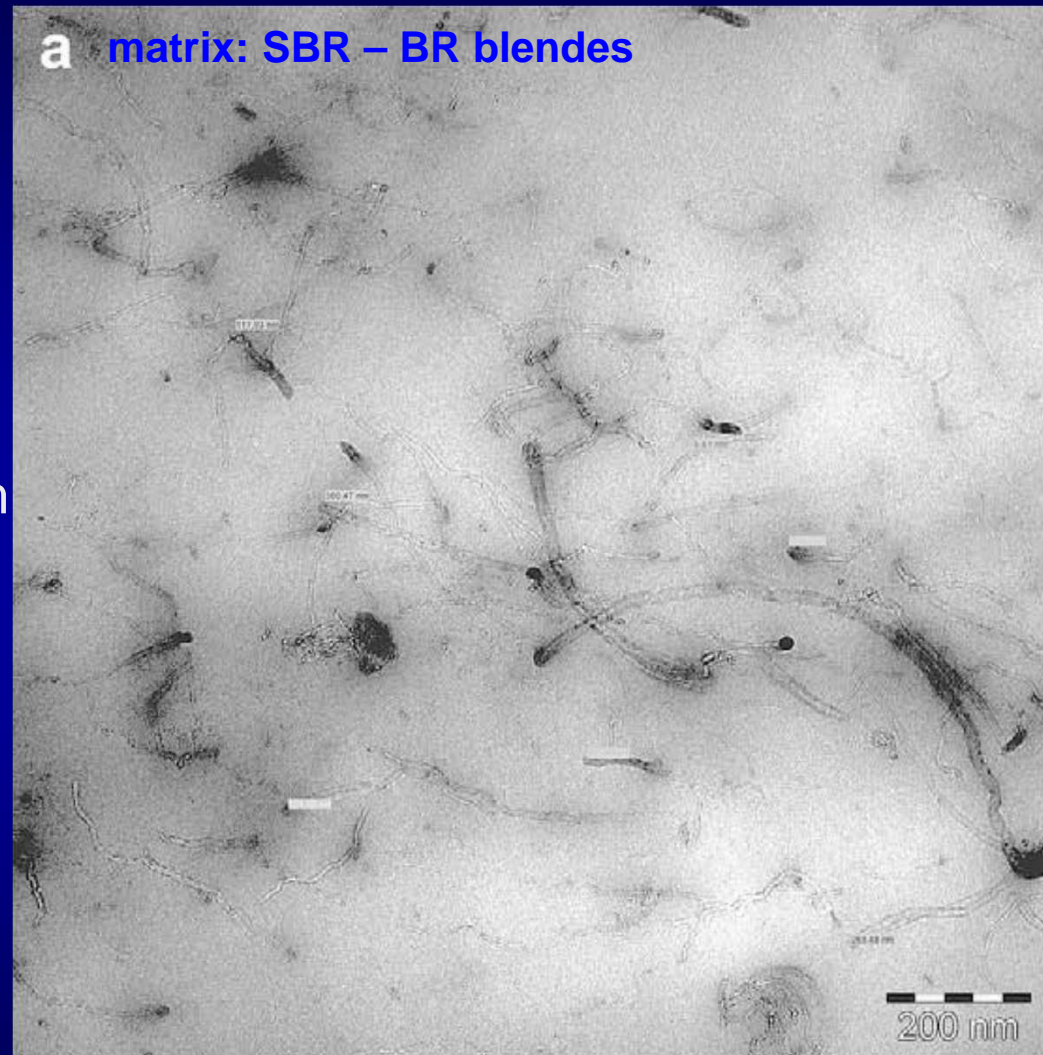
CNT/EtOH

Improvement of CNT dispersion

Diameter of tube: 6 – 27nm

Length of tubes:
from a few to several hundred nm

CNT percolation
at 5 phr

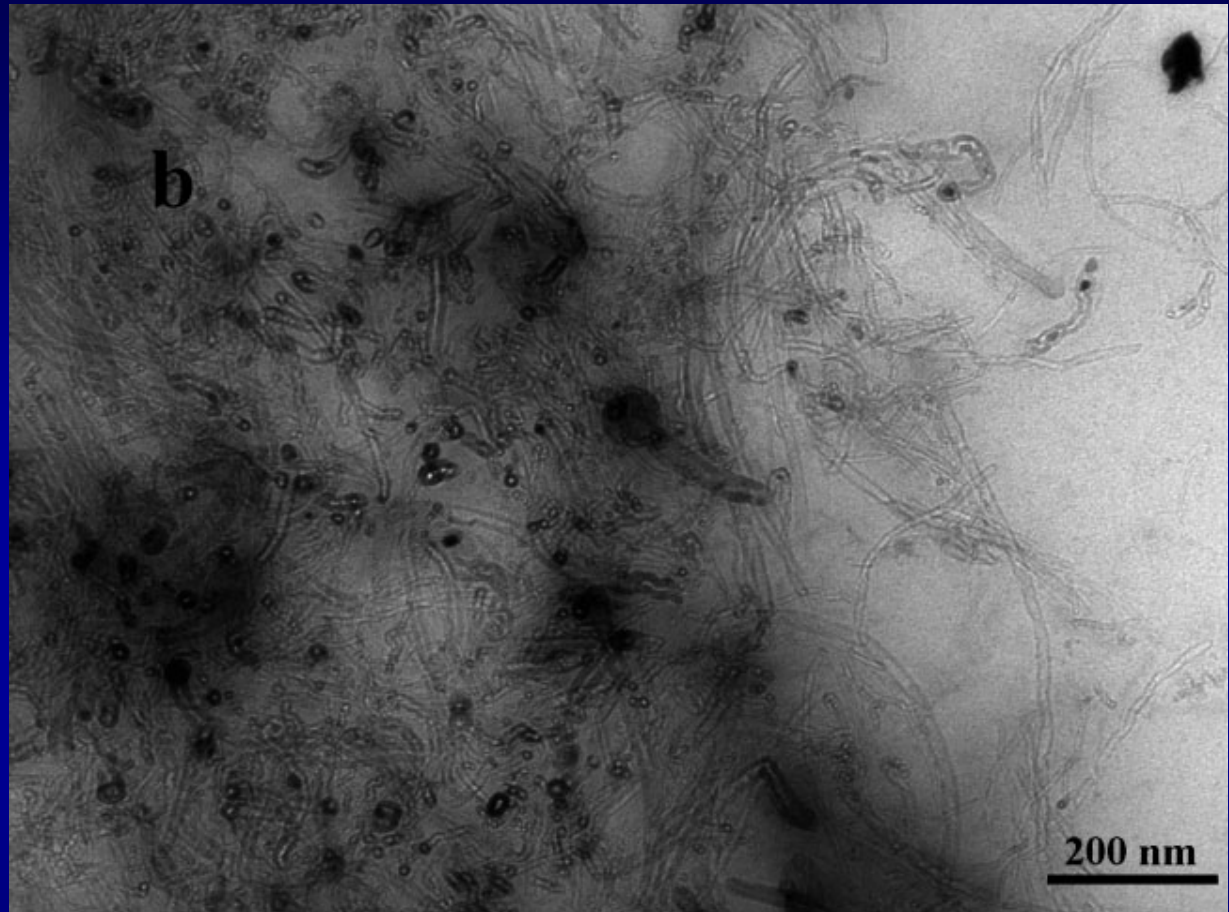


A. Das, K.W. Stockelhuber, R. Jurk, M. Saphiannikova, J. Fritzsche, H. Lorenz, M. Kuppler, G. Heinrich
Polymer 2008, 49, 5276 - 5283

Composites from solution blending

Improvement of CNT dispersion

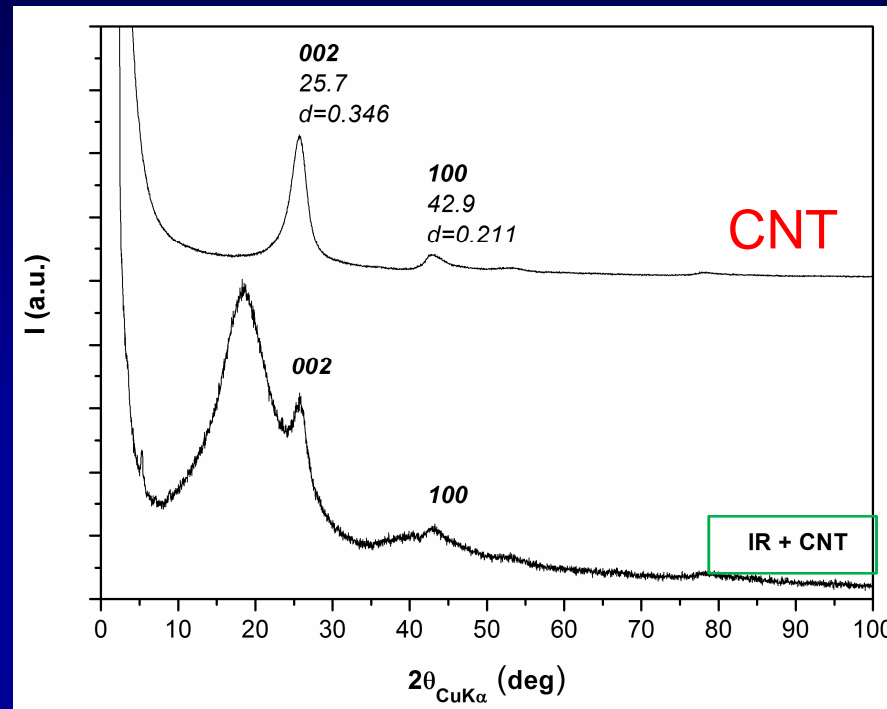
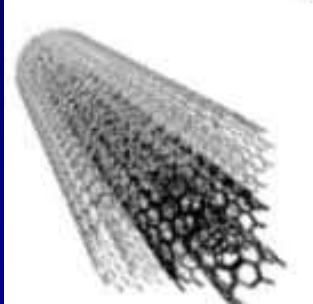
Presence of both individual and
agglomerates of CNT



NR / CNT 3.8 wt%

L. Bokobza, and M. Kolodziej
Polym Int 2006, 55, 1090 - 1098

Crystalline structure of CNT



XRD analysis

IR 100, CNT 11

Scherrer equation: $D_{hkl} = 0.9 \lambda / \beta_{hkl} \cos\theta_{hkl}$

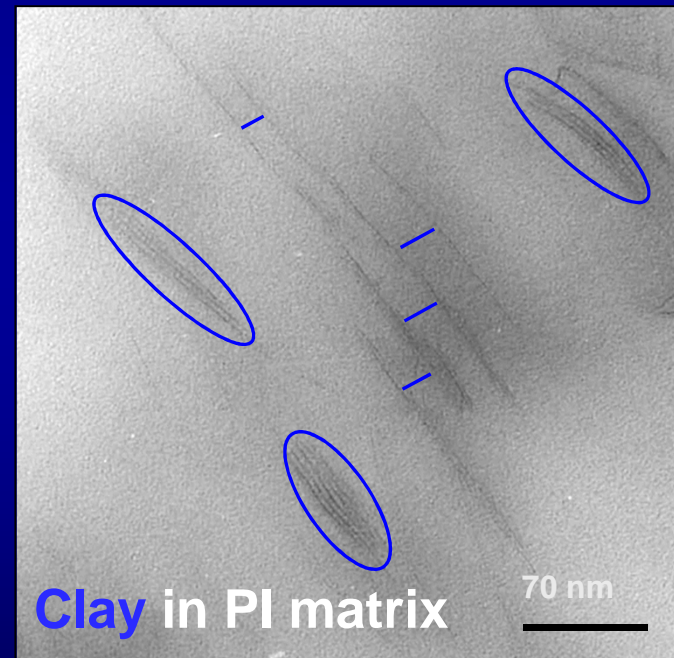
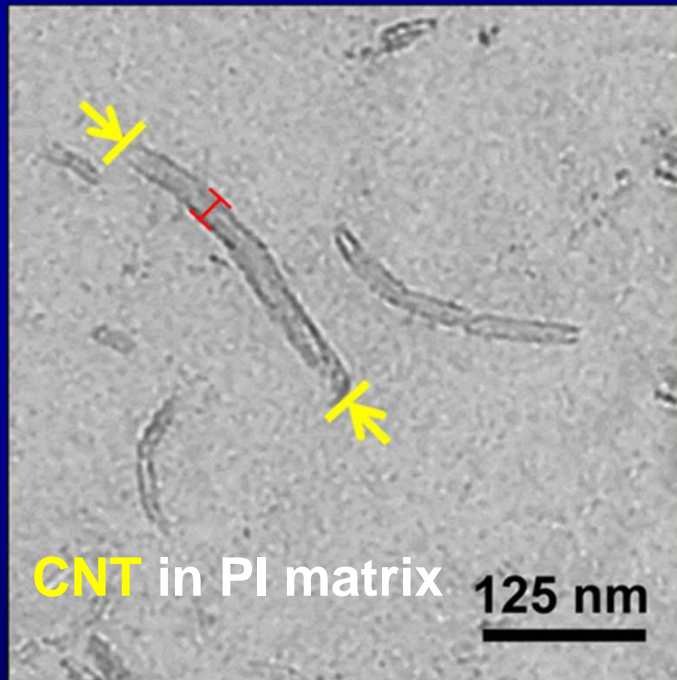
Sample	d_{002} (nm)	D_{002} (nm)	N° piled layer
IR + CNT	0.346	~ 5	~ 15
CNT	0.346	3.7	10

M. Galimberti, M. Coombs, V. Cipolletti, L. Giannini, T. Riccò, S. Pandini, L. Conzatti, M. Mauro, G. Guerra
Presented at 181th Technical Meeting of the Rubber Division of ACS, San Antonio (TX), April 22-25, 2012

Aspect ratio of CNT

Aspect ratio

defined as the ratio of length to diameter for a **fiber, such as CNT** or the ratio of diameter to thickness for **platelets, such as clay**.



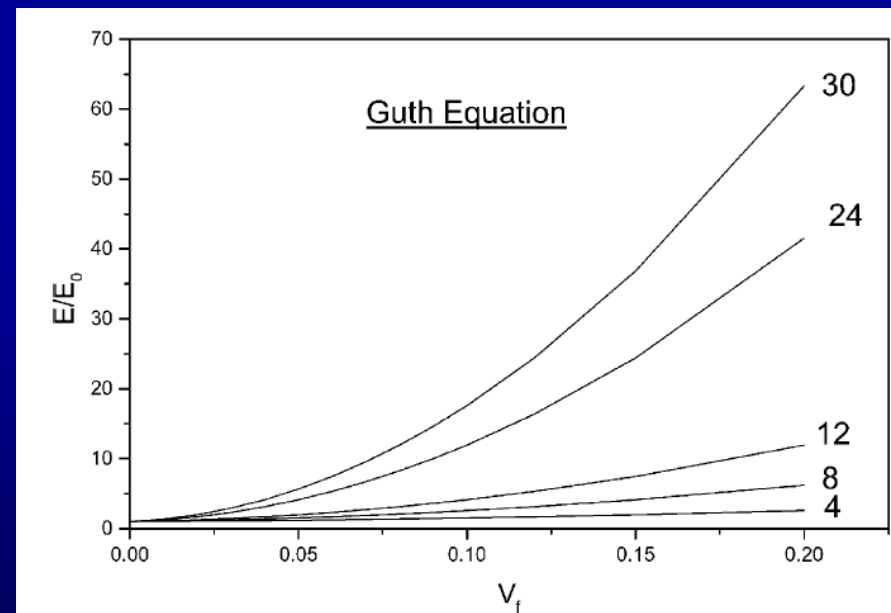
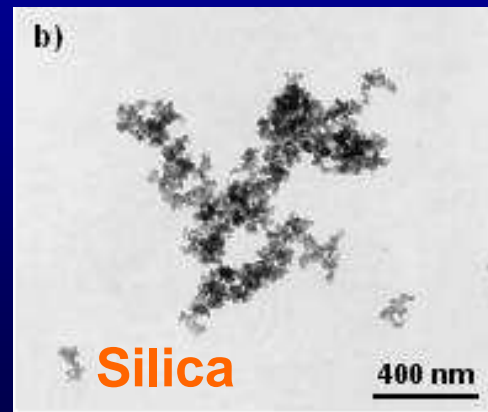
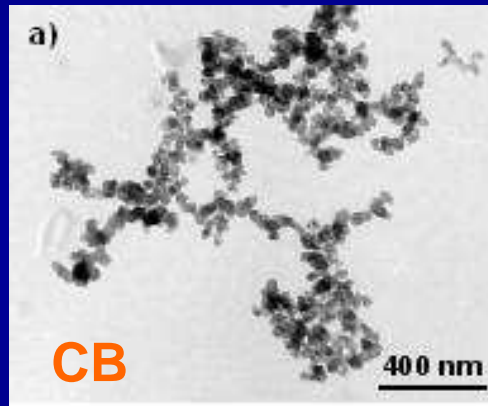
TEM micrographs taken at ISMAC-CNR Genova, L. Conzatti

Aspect ratio of CNT in polymer composites

Why is important?

The Guth equation

$$E = E_m (1 + 0.67 f \Phi + 1.62 f^2 \Phi^2)$$



Aspect ratio of CNT in polymer composites

CNT aspect ratio from Guth equation

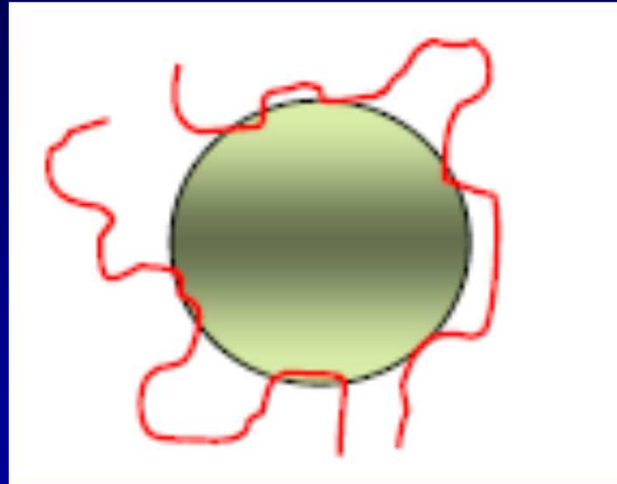
The Guth equation

$$E = E_m (1 + 0.67 f \Phi + 1.62 f^2 \Phi^2)$$

Polymer	f value	ref.
blend poly(1,4-cis-butadiene) / poly(styrene-co-butadiene)	15 - 20	A. Das, K. W. Stöckelhuber, R. Jurk, M. Grenzer, J. Fritzsche, H. Lorenz, M. Klüppel, G. Heinrich, <i>Polymer</i> 2008 , 49(24), 5276-83
poly(styrene-co-butadiene)	40 - 45	L. Bokobza, <i>Polymer</i> . 2007 , 48, 4907-20
poly(isoprene)	22	Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I. <i>Macromol. Mater. Eng.</i> 2012, 298(2), 241-251

CNT – polymer interface

CNT – polymer interface

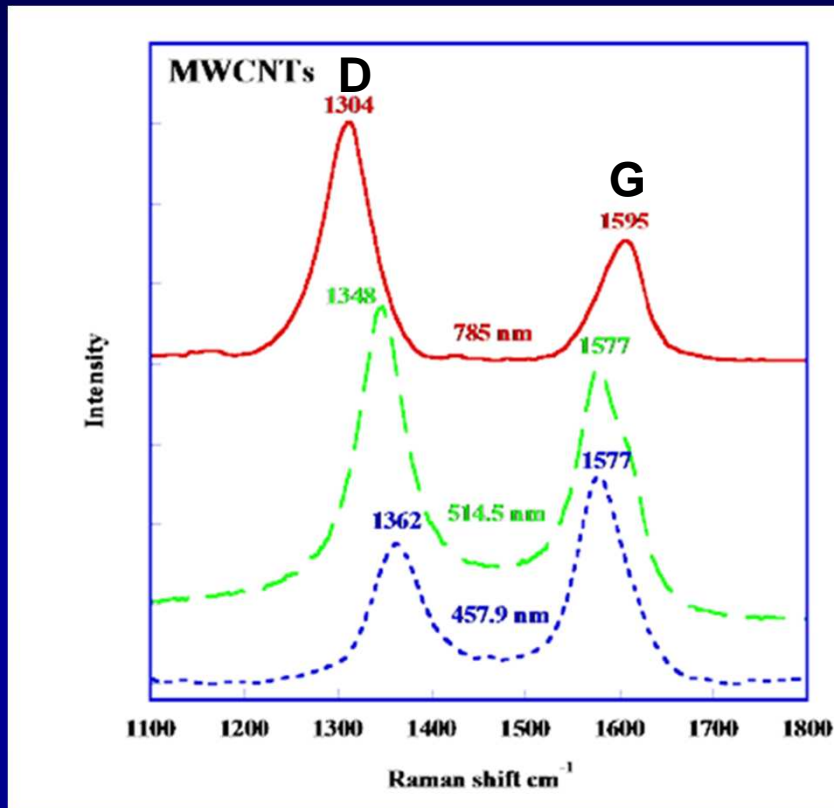


Filler-rubber interaction

Techniques used to study filler-polymer interface

- Solid-state NMR Spectroscopy
- Bound Rubber
- DSC: T_g
- Raman Spectroscopy

CNT – polymer interface



- **G band**
in-plane vibration of C–C bond
- **D band**
activated by the presence of disorder in carbon systems.

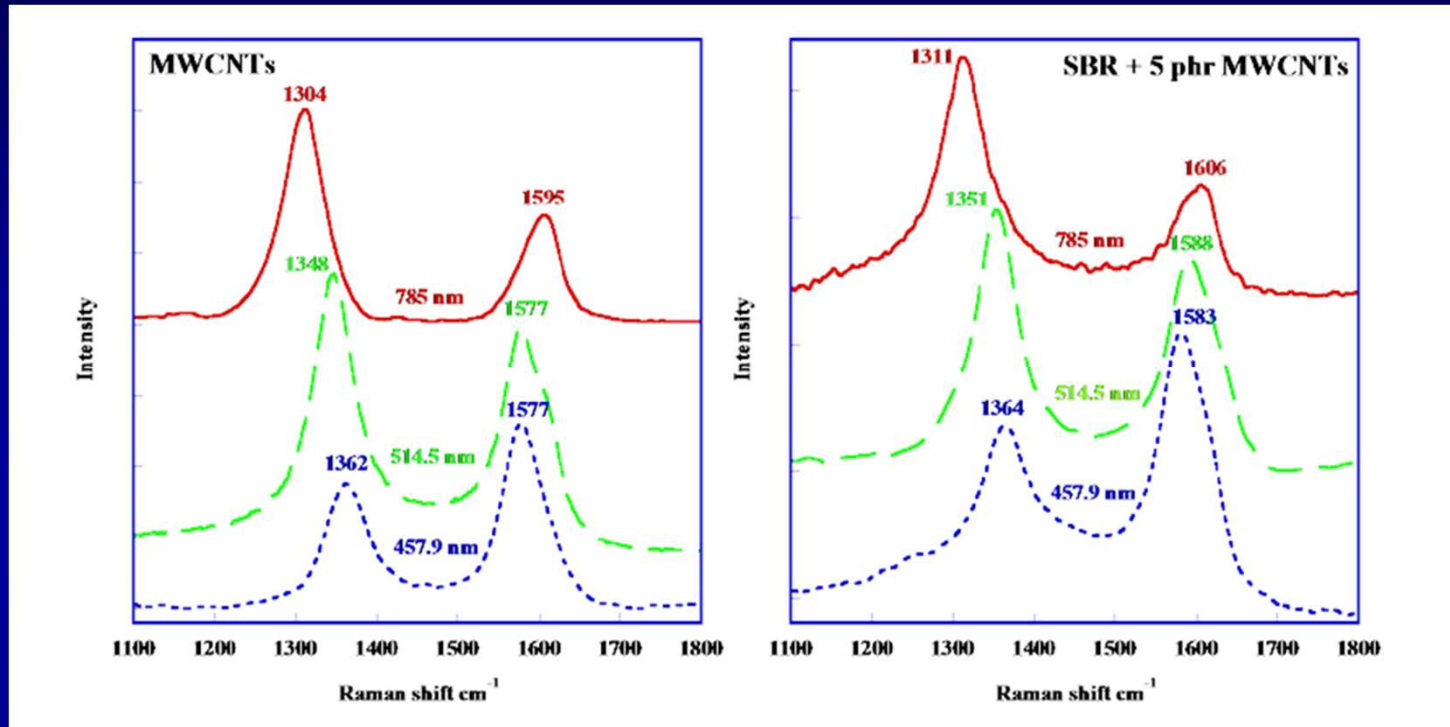
Raman spectra of CNT obtained with laser wavelengths 457.9, 514.5 and 785 nm

L. Bokobza

Presented at 181th Technical Meeting of the Rubber Division of ACS, San Antonio (TX)

April 22-25, 2012

CNT – polymer interface



upshifting

disentanglement and subsequent dispersion
in the polymeric medium

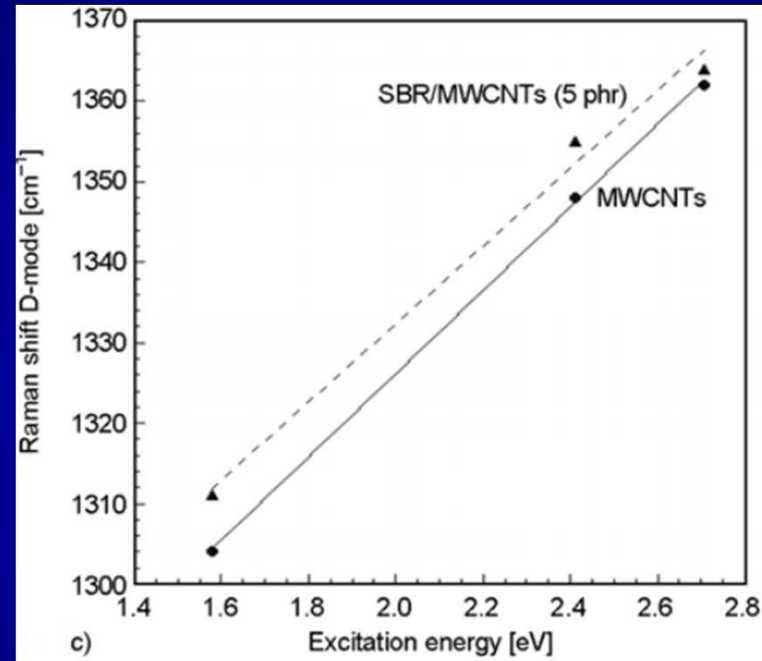
L. Bokobza

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CNT – polymer interface

Dependence of the wavenumber of the D band on laser energy

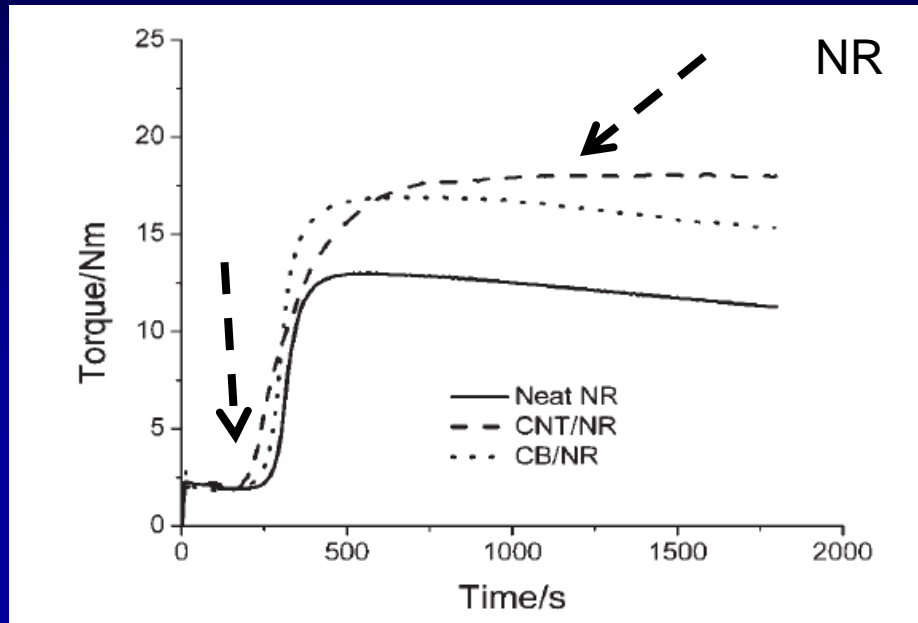


The wavenumber of the D band increases with increasing laser energy

L. Bokobza*, J. Zhang *eXPRESS Polymer Letters Vol.6, No.7 (2012) 601–608*

Properties of CNT based nanocomposites

Vulcanization behaviour



CB, CNT = 25 phr

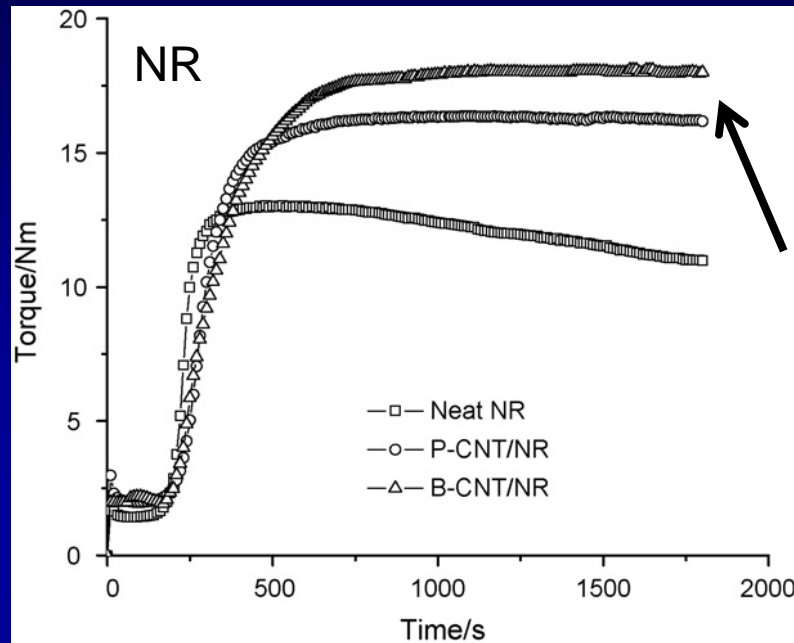
Reduction of scorch time
due to enhanced thermal conductivity

Higher Modulus

	Neat NR	CNT/NR	CB/NR
	phr	phr	phr
NR	100	100	100
Zinc Oxide	5	5	5
Stearic Acid	3	3	3
Sulfur	2,8	2,8	2,8
N-Cyclohexyl-2-benzothiazole-sulfenamide	1,3	1,3	1,3
2-Mercaptobenzothiazole	0,1	0,1	0,1
Ball-milled CNTs	0	25	0
CB	0	0	25

Sui, G.; Zhong, W. H.; Yang, X. P.; Yu, Y. H.; Zhao, S. H.
Polymers for Advanced Technologies (2008),19(11), 1543-1549

Vulcanization behaviour



CB, CNT = 25 phr

P-CNT = Purified CNT

B-CNT = Ball-milled CNT

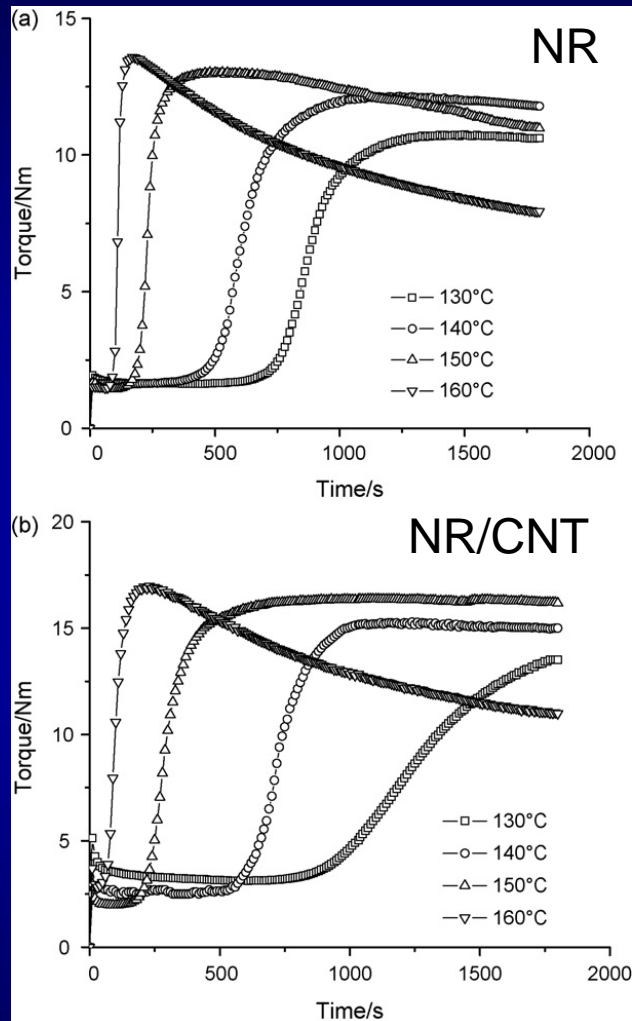
Slight increase in scorch time

Higher modulus

G. Sui, W. H. Zhong, X. P. Yang, Y. H. Yu, S. H. Zhao
Mater. Sci. Eng.: A 485, 524 (2008).

	Neat NR	P-CNT/NR	P-CNT/NR
	<i>phr</i>	<i>phr</i>	<i>phr</i>
NR	100	100	100
Zinc Oxide	5	5	5
Stearic Acid	3	3	3
Sulfur	2,8	2,8	2,8
N-Cyclohexyl-2-benzothiazole-sulfenamide	1,3	1,3	1,3
2-Mercaptobenzothiazole	0,1	0,1	0,1
Purified CNTs	0	25	0
Ball-Milled CNTs	0	0	25

Vulcanization behaviour



Sample	Activation energy (kJ/mol)
Neat NR	58.51
P-CNT/NR	90.96

Higher activation energy
due to absorption of accelerators
on CNT

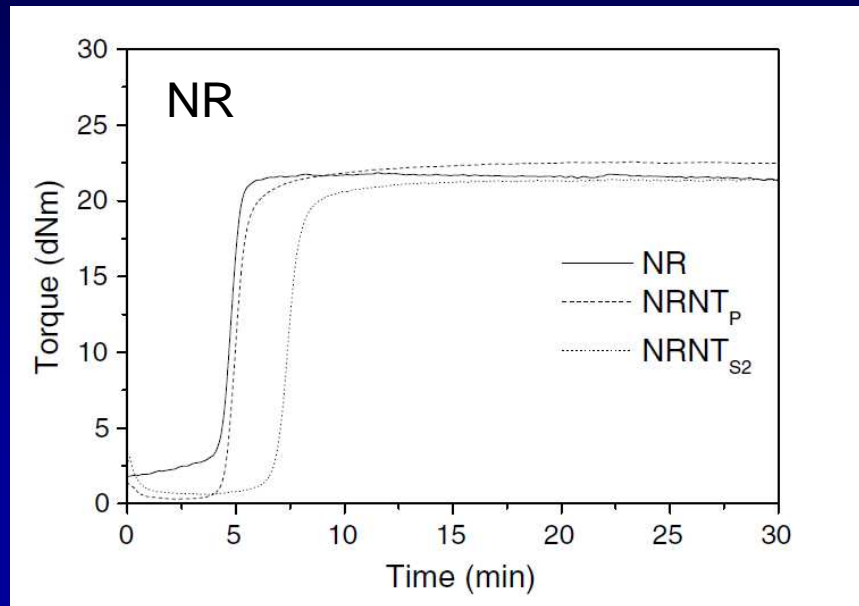
Higher modulus

CNT = 25 phr

	Neat NR	P-CNT/NR	P-CNT/NR
	<i>phr</i>	<i>phr</i>	<i>phr</i>
NR	100	100	100
Zinc Oxide	5	5	5
Stearic Acid	3	3	3
Sulfur	2,8	2,8	2,8
N-Cyclohexyl-2-benzothiazole-sulfenamide	1,3	1,3	1,3
2-Mercaptobenzothiazole	0,1	0,1	0,1
Purified CNTs	0	25	0
Ball-Milled CNTs	0	0	25

G. Sui, W. H. Zhong, X. P. Yang, Y. H. Yu, S. H. Zhao
Mater. Sci. Eng.: A 485, 524 (2008).

Vulcanization behaviour



CNT = 1 phr

Rubber: NR,
 NRNT_P = with pristine CNT
 NRNT_{S2} = with functionalized CNT

Scorch time increase for NRNT_P or NRNT_{S2}

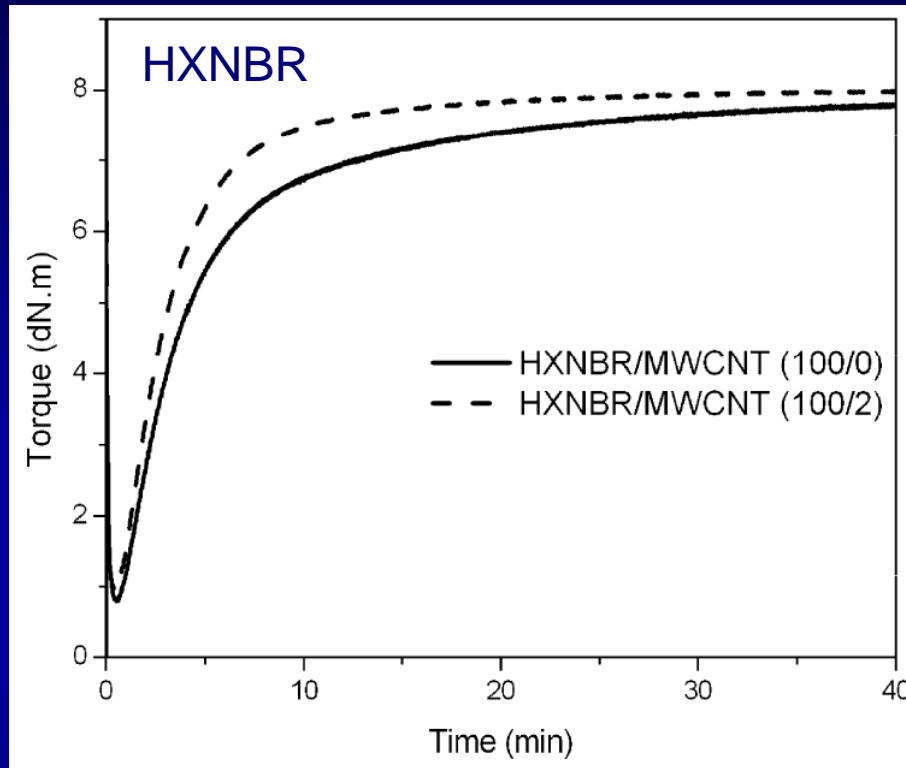
Further scorch time increase for CNT with COOH groups

Higher Modulus

	Amounts
	phr
NR	100
Zinc Oxide	5
Stearic Acid	2
Antioxidant (Polymerized trimethyl quinoline)	1
Multiwall carbon nanotube	1
MBTS	1,2
TMT	0,6
Sulfur	2,5

M. Shanmugaraj, J. H. Bae, K. Y. Lee, W. H. Noh, S. H. Lee, S. H. Ryu,
Compos. Sci. Technol. 67, 1813 (2007).

Vulcanization behaviour



HXNBR
33% AN,
5% COOH
3.5% residual double bonds

CNT = 0, 1, 2 and 4 phr

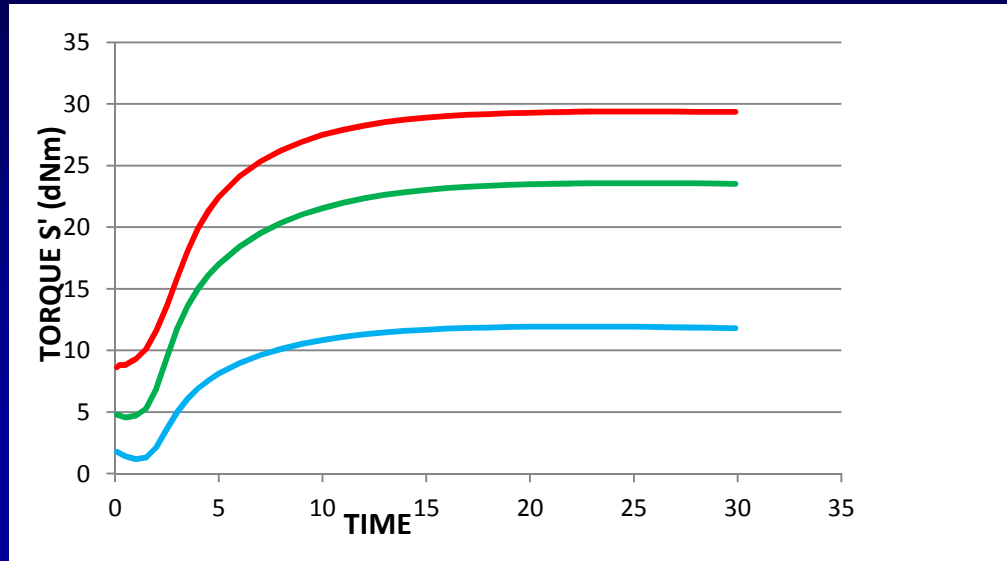
DCP = 3 phr

Shorter scorch due to the increase of thermal conductivity

Higher Modulus

L. Lu, Y. Zhai, Y. Zhang, C. Ong, S. Guo
APPL. SURF. SCI. **255**, 2162 (2008).

Vulcanization behaviour



	GR ' RAW' + CB	GR ' RAW' + CNT	GR ' RAW' + 50CNT/50CB
	phr	phr	phr
NR	100	100	100
CB - N 326	35	0	17,5
CNT	0	35	17,5
Zinc Oxide	6	6	6
Stearic Acid	0,5	0,5	0,5
Sulfur	3,5	3,5	3,5
TBBS	0,7	0,7	0,7

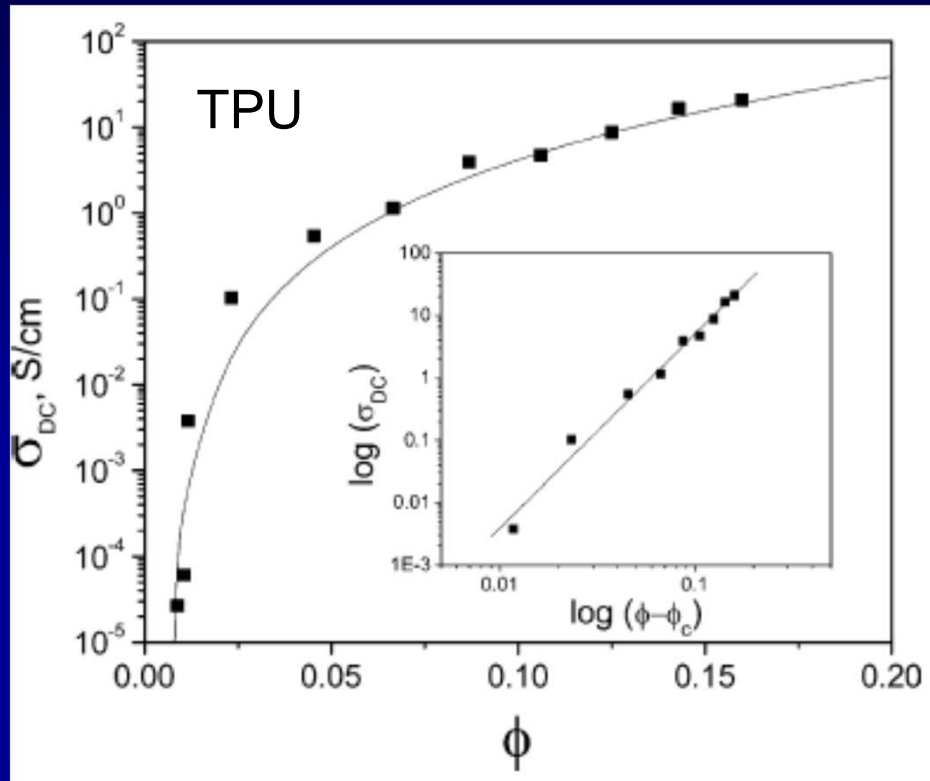
Shorter scorch

Higher Modulus

	NR + CB	NR + CNT	NR + CNT _{50%} /CB _{50%}
MAXIMUM TORQUE (dNm)	11,94	29,4	23,61
t (1) min	2,01	1,25	1,67
t (90) min	7,27	3,65	4,9

S. Musto, M. Galimberti
Unpublished results

Electrical Conductivity



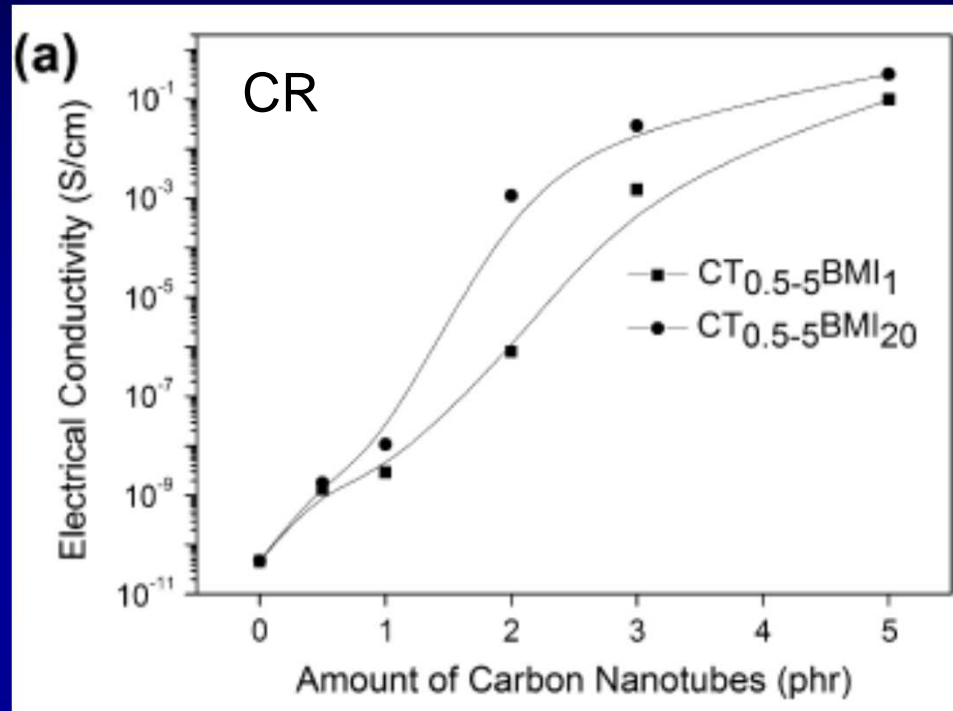
MWCNT \approx 0.5 – 10 Vol%

Low electrical Percolation
 ϕ (volume fraction) \sim 0.005

Conductivity
 $\sigma \sim$ 1-10 S/cm

Hilmar Koerner, Weidong Liu, Max Alexander, Peter Mirau, Heather Dowty, Richard A. Vaia
Polymer (2005), 46, 4405 -4420

Electrical Conductivity



BMI = ionic liquid

Percolation Threshold

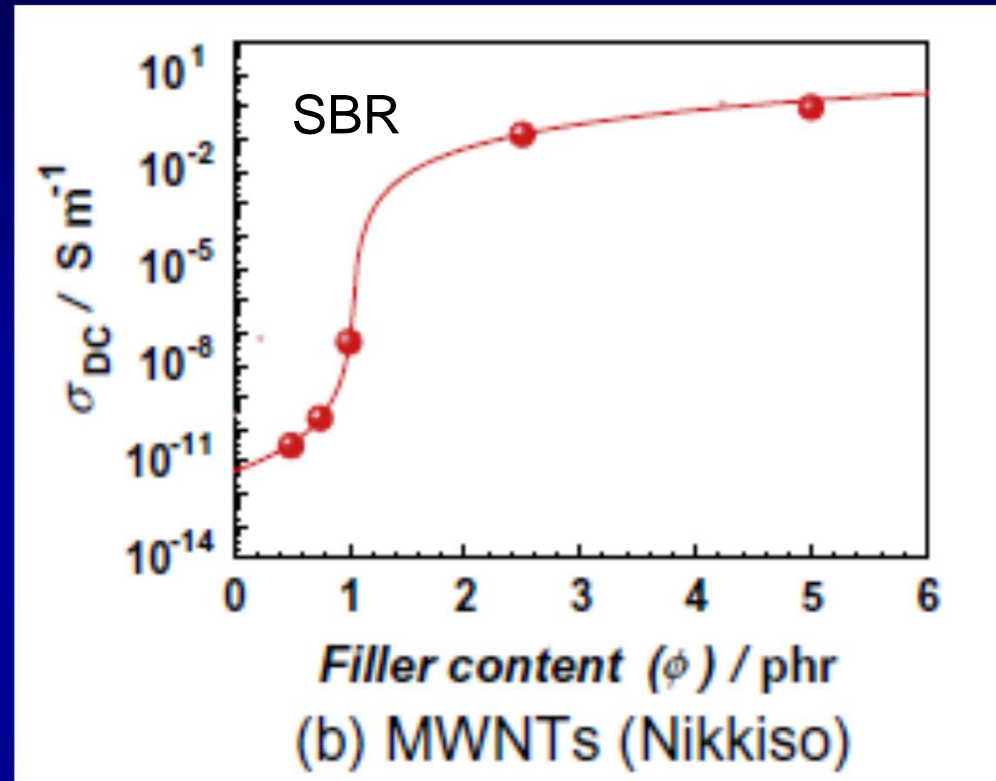
1 - 3 phr

Conductivity

$\sigma_{DC} \sim 10^{-1}$ S/cm

Kalaivani Subramaniam, Amit Das, Gert Heinrich
Composites Science and Technology (2011), 71, 1441 - 1449

Electrical Conductivity



Percolation Threshold

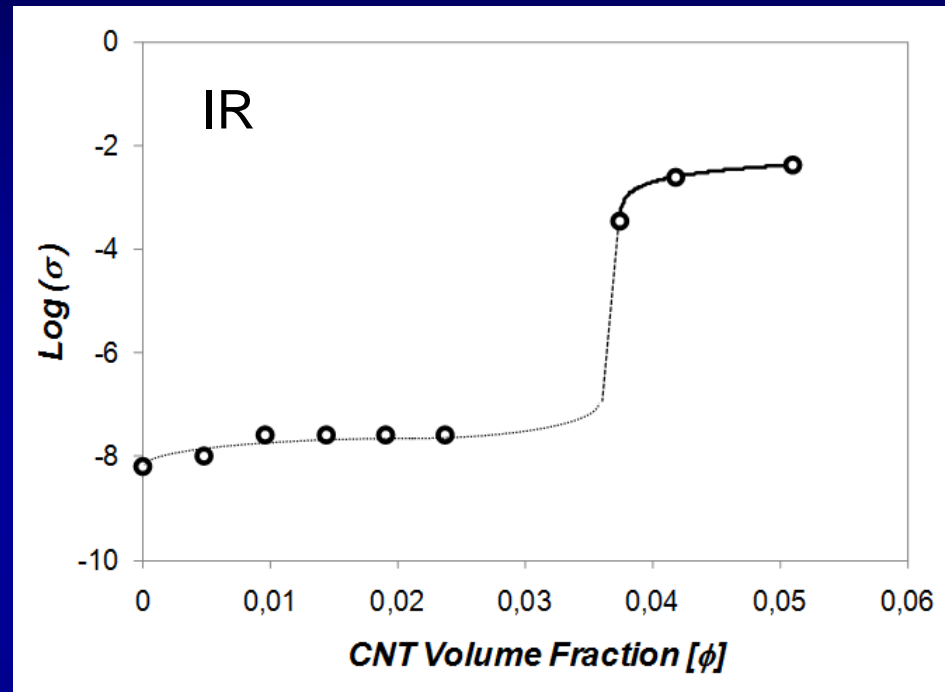
$$\varphi_c \approx 0.95 \text{ phr}$$

Conductivity

$$\sigma_{DC} \sim 5 \cdot 10^{-2} \text{ S/cm}$$

Koji Tsuchiya, Ayumu Sakai, Tomoya Nagaoka, Katsumi Uchida, Takeo Futukawa, Hirofumi Yajima
Composites Science and Technology (2011), 71, 1098 - 1104

Electrical Conductivity

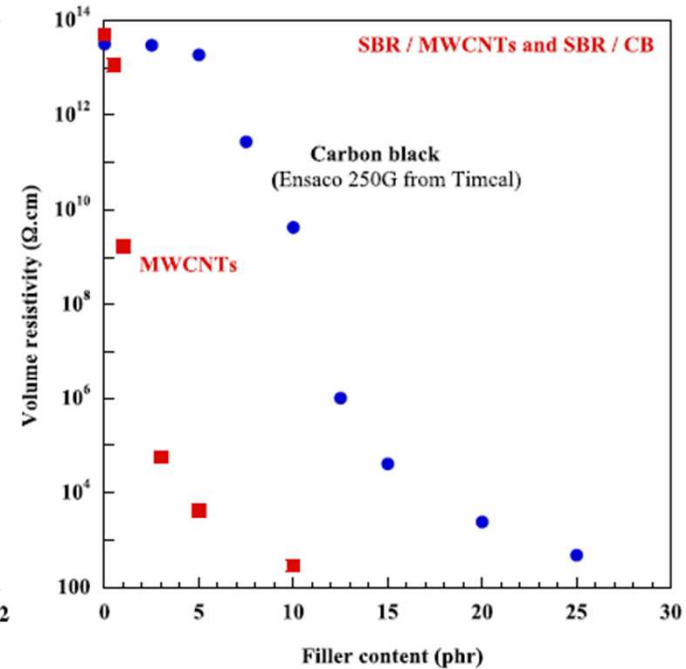
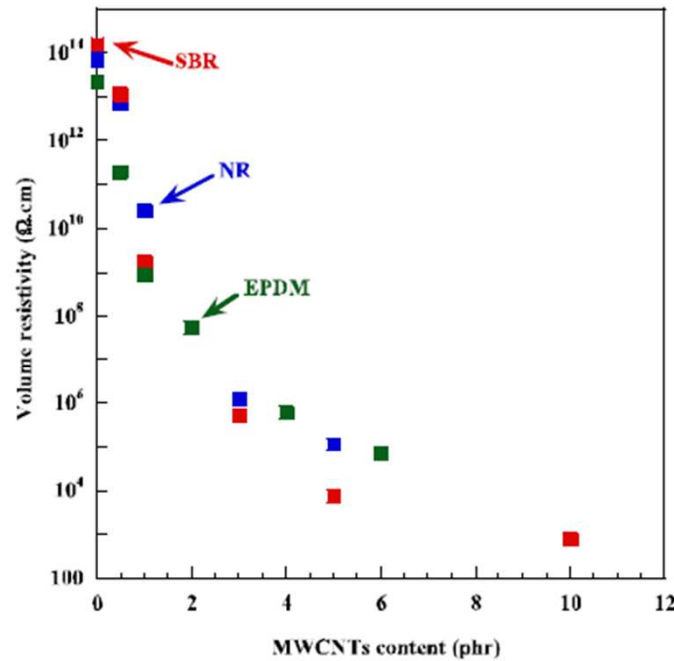
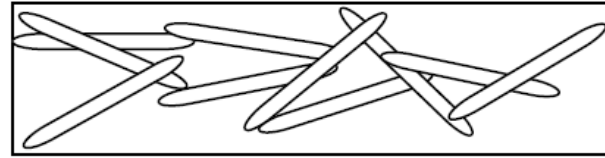
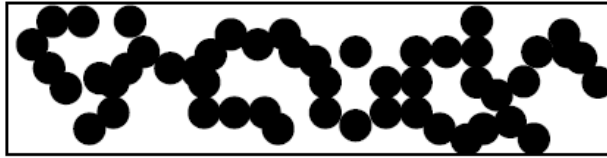


Percolation Threshold
 ϕ_c (volume fraction) ≈ 0.037

Conductivity
 $\sigma_{DC} \approx 10^{-2}$ S/m

Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
Macromol. Mater. Eng. 2012, 298(2), 241-251

Electrical conductivity



Percolation threshold at ~ 0.5 phr (vol. fraction ~ 0.002)

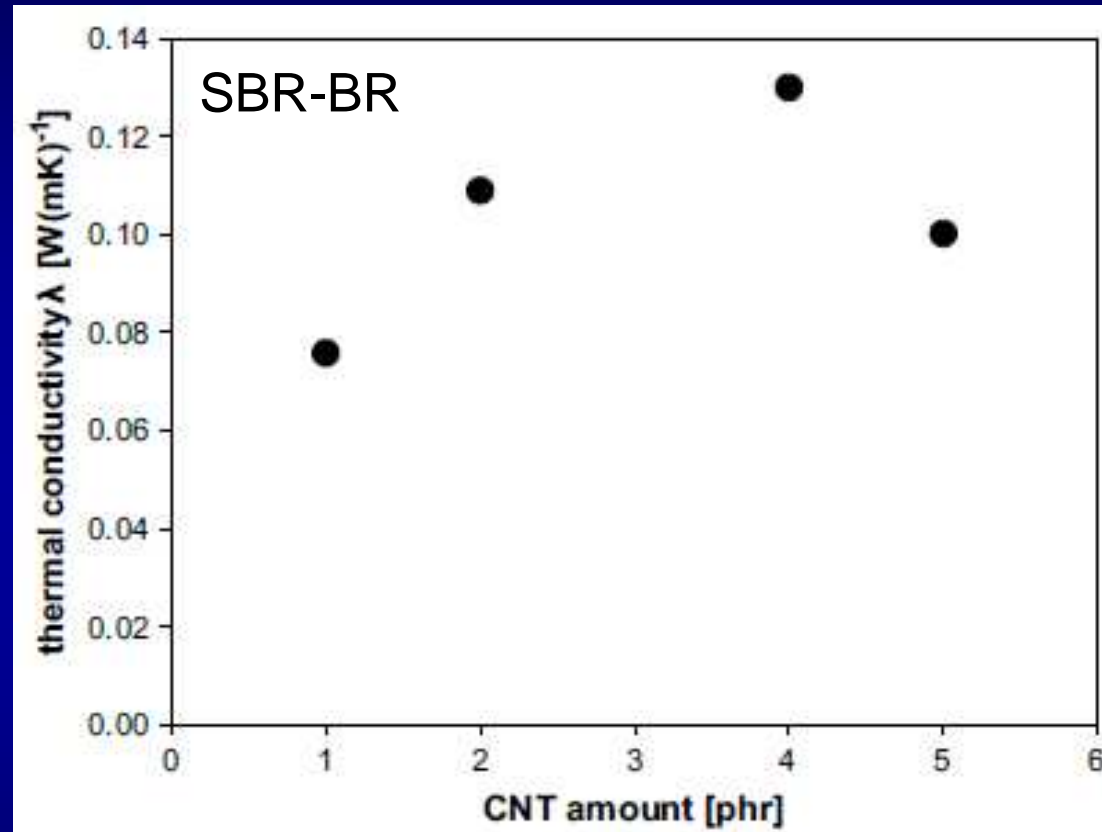
L. Bokobza

Presented at 181th Technical Meeting of the Rubber Division of ACS, San Antonio (TX)

April 22-25, 2012

Thermal Conductivity

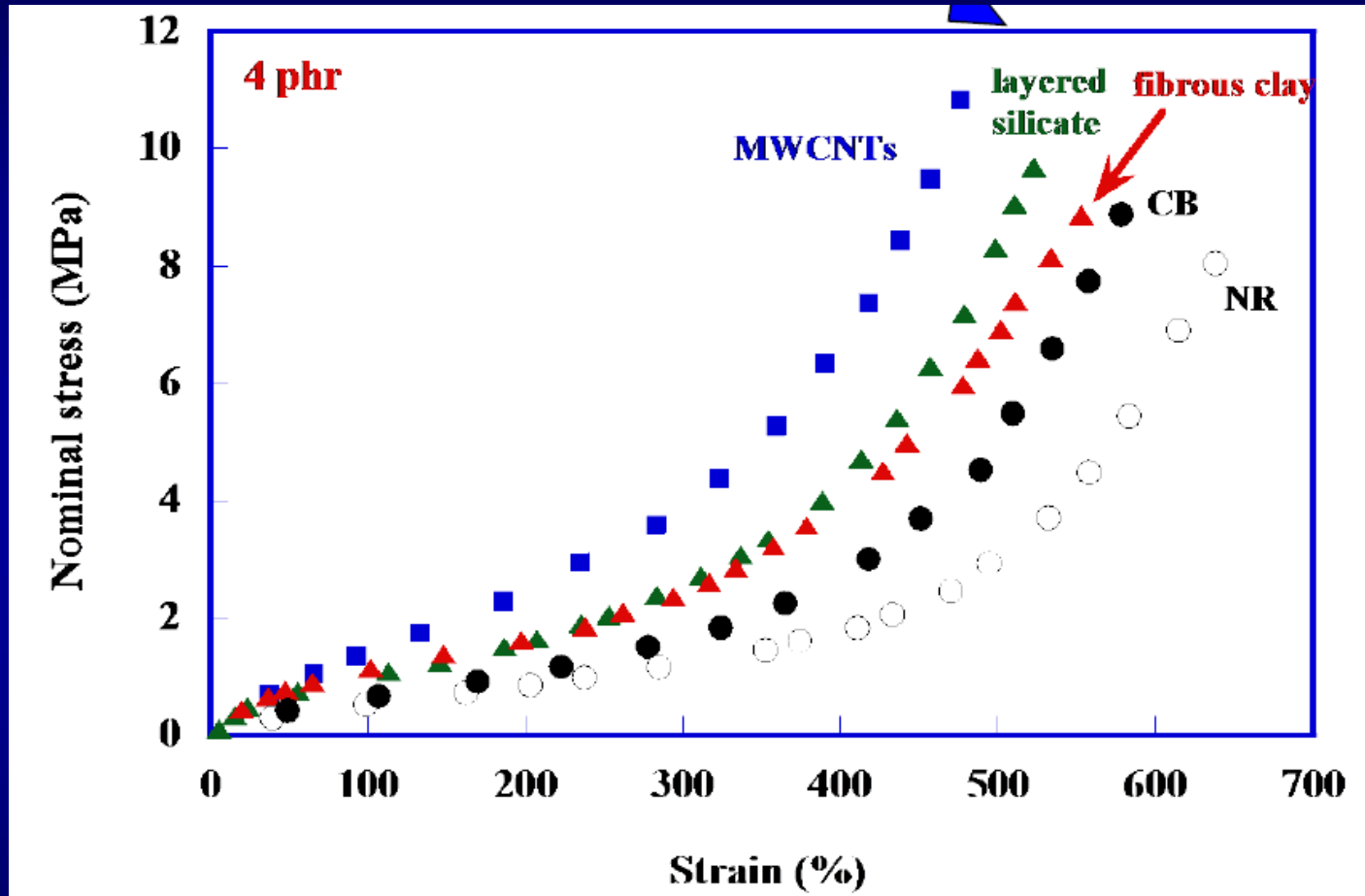
CNT (*Wet* melt blending)



Slight enhancement

A. Das, K.W. Stockelhuber, R. Jurk, M. Saphiannikova, J. Fritzsche, H. Lorenz, M. Kuppler, G. Heinrich
Polymer 2008, 49, 5276 - 5283

Mechanical Properties



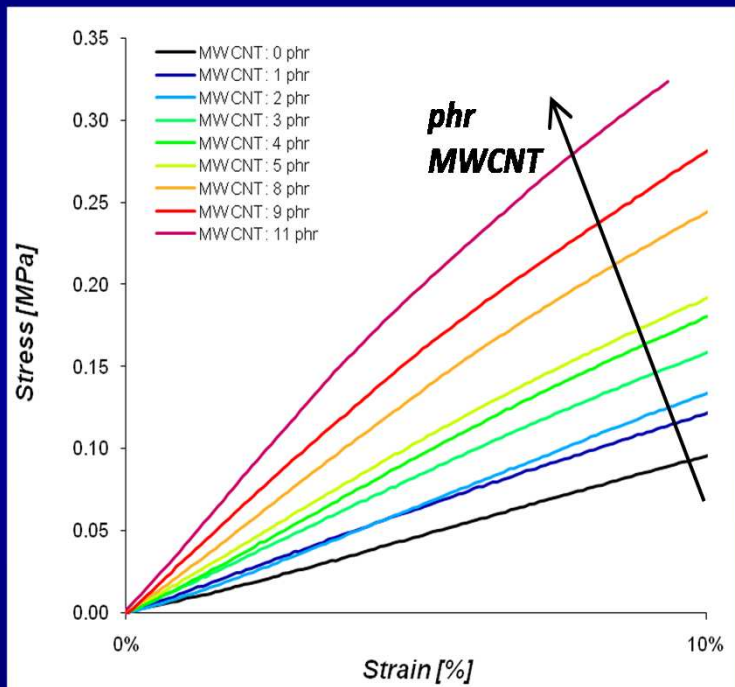
L. Bokobza

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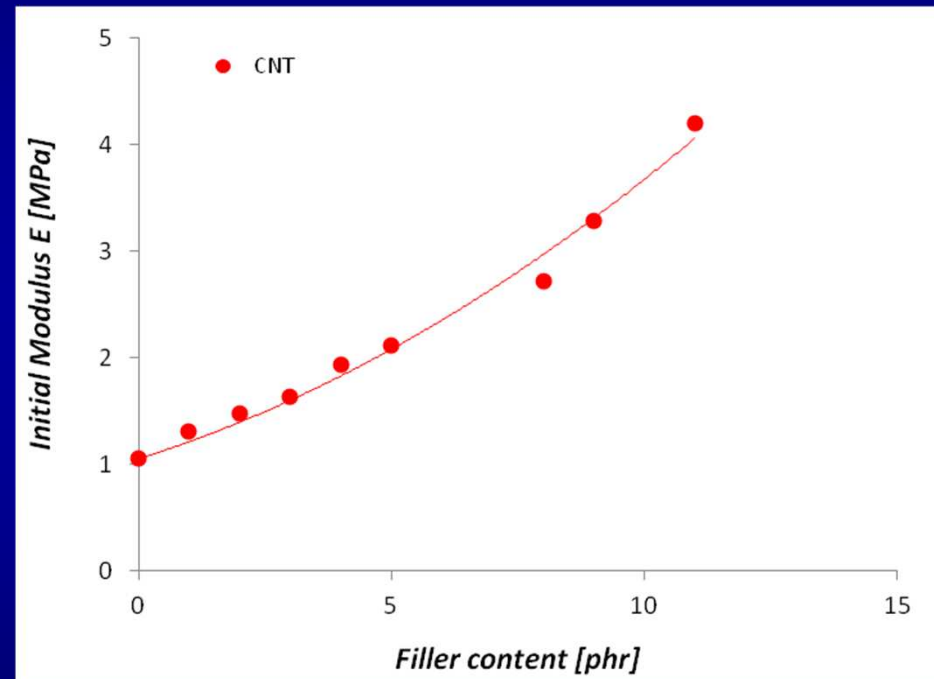
April 22-25, 2012

Mechanical Properties

Stress strain curves



E Initial modulus from stress strain curves

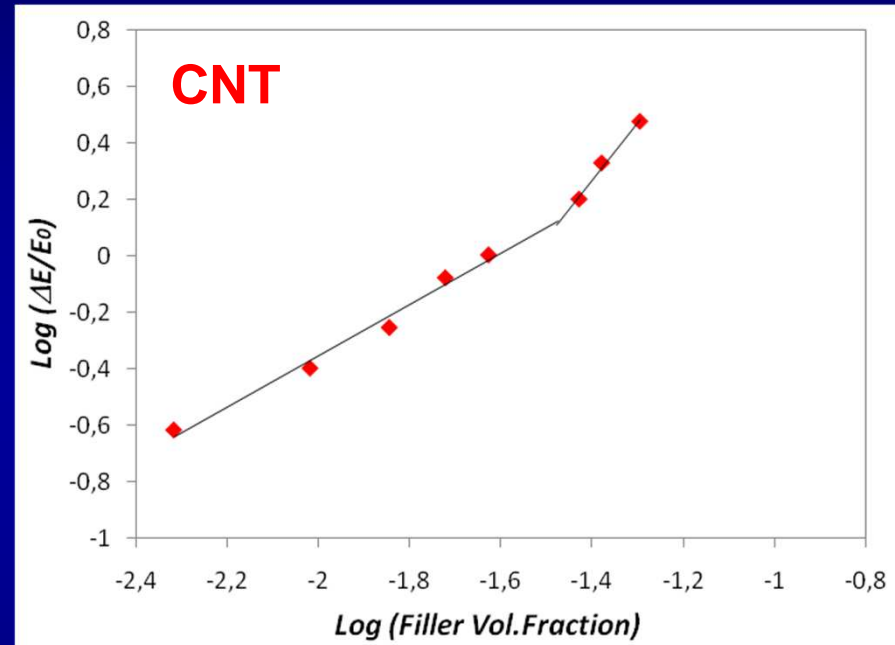


Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
Macromol. Mater. Eng. 2012, 298(2), 241-251

Mechanical Properties

Filler percolation threshold

Hüber – Vilgis plots*



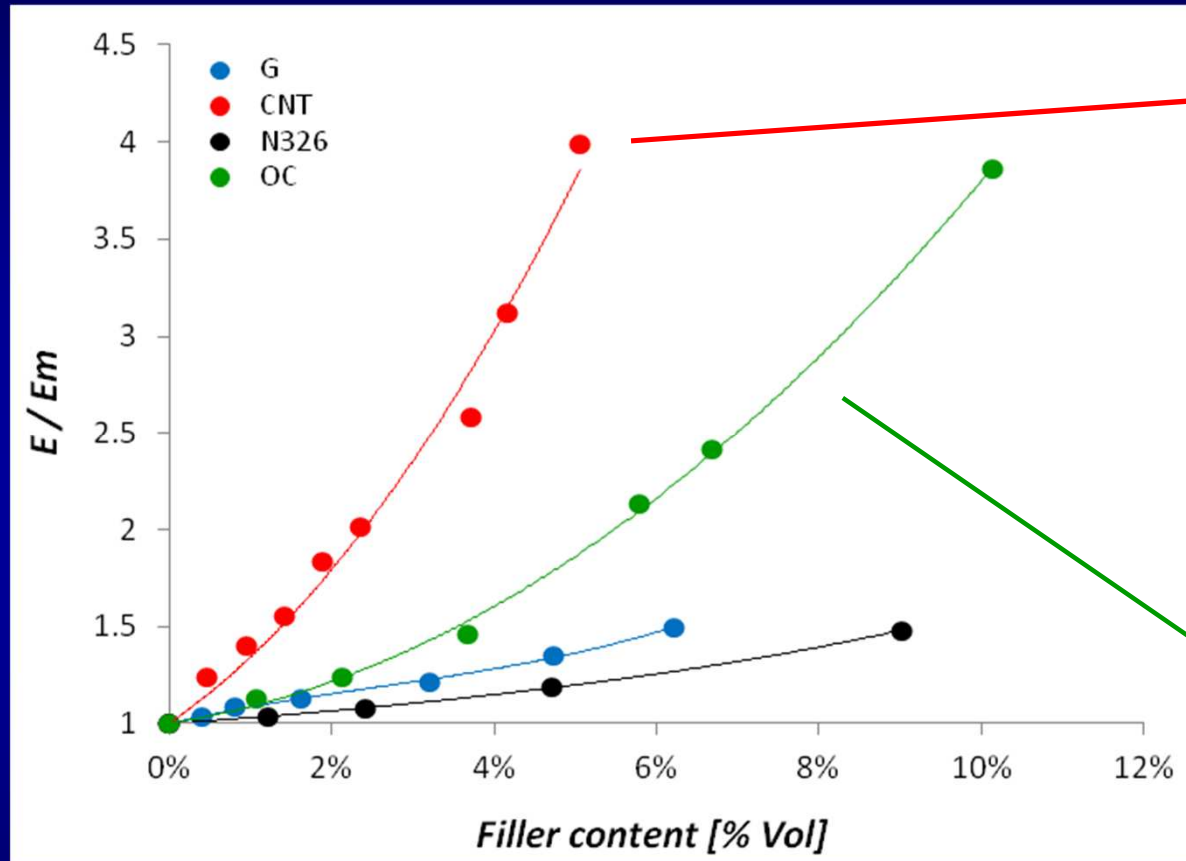
$$\phi = 0.034 \quad \text{phr} = 7.2$$

Galimberti M. et al.
Macromol. Mater. Eng. 2012, 298(2), 241-251

* Huber G., Vilgis T.A.,
Kaut Gummi Kunstst 52(2) (1999) 102-7

Mechanical Properties

E initial modulus vs. Filler content



From Guth
Equation:
 $f_{CNT} = 22$

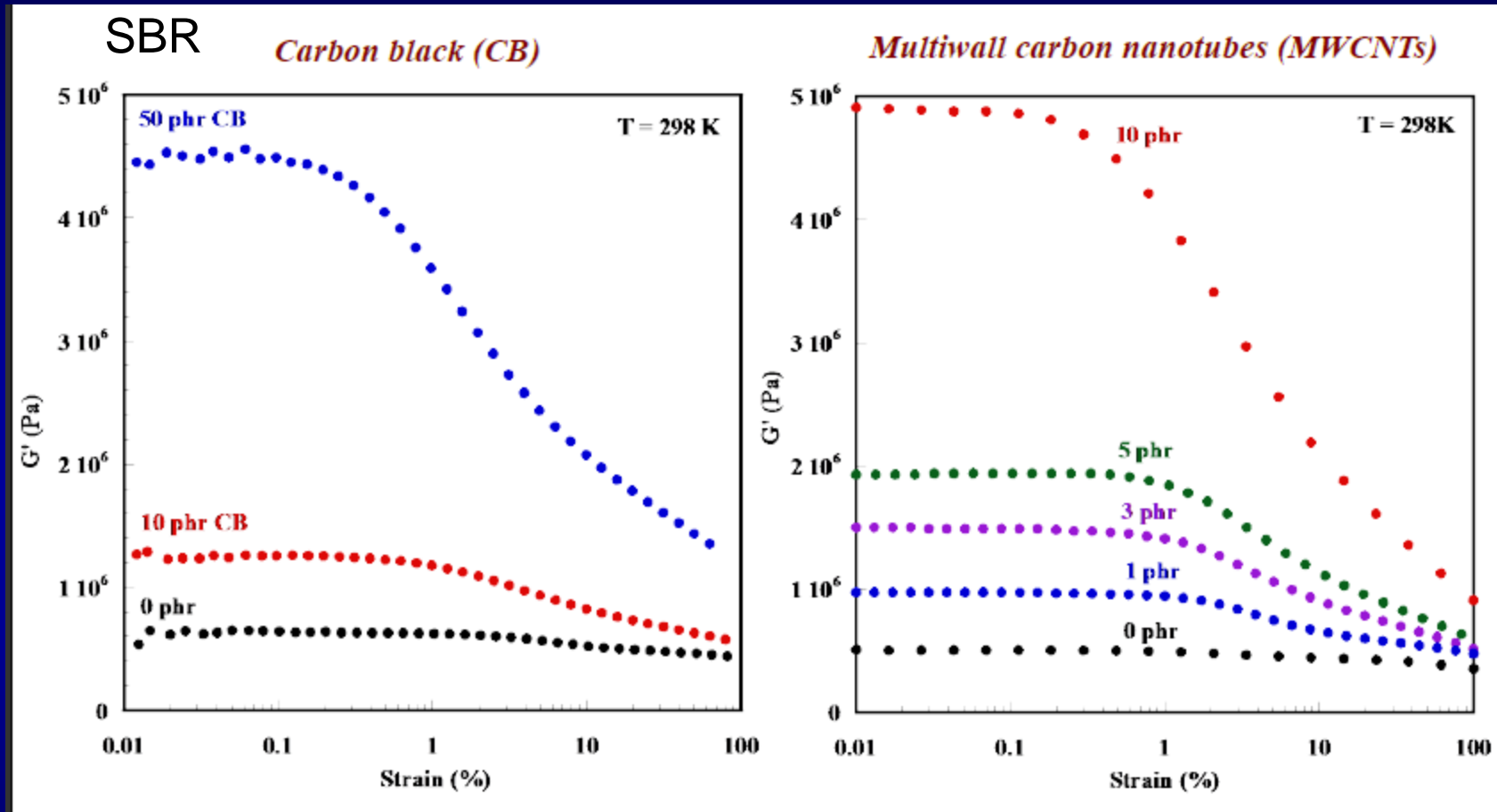
From Guth
Equation:
 $f_{OC} = 11.5$

Galimberti M., Coombs M., Cipolletti V., Riccio P., Ricco` T., Pandini S., Conzatti L.,
Applied Clay Science 65–66 (2012) 57–66

Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
Macromol. Mater. Eng. 2012, 298(2), 241-251

M. Galimberti, V. Kumar, M. Coombs, V. Cipolletti, S. Agnelli, S. Pandini, L. Conzatti,
Rubber Chem. Technol. in press

Non linearity of dynamic mechanical behaviour

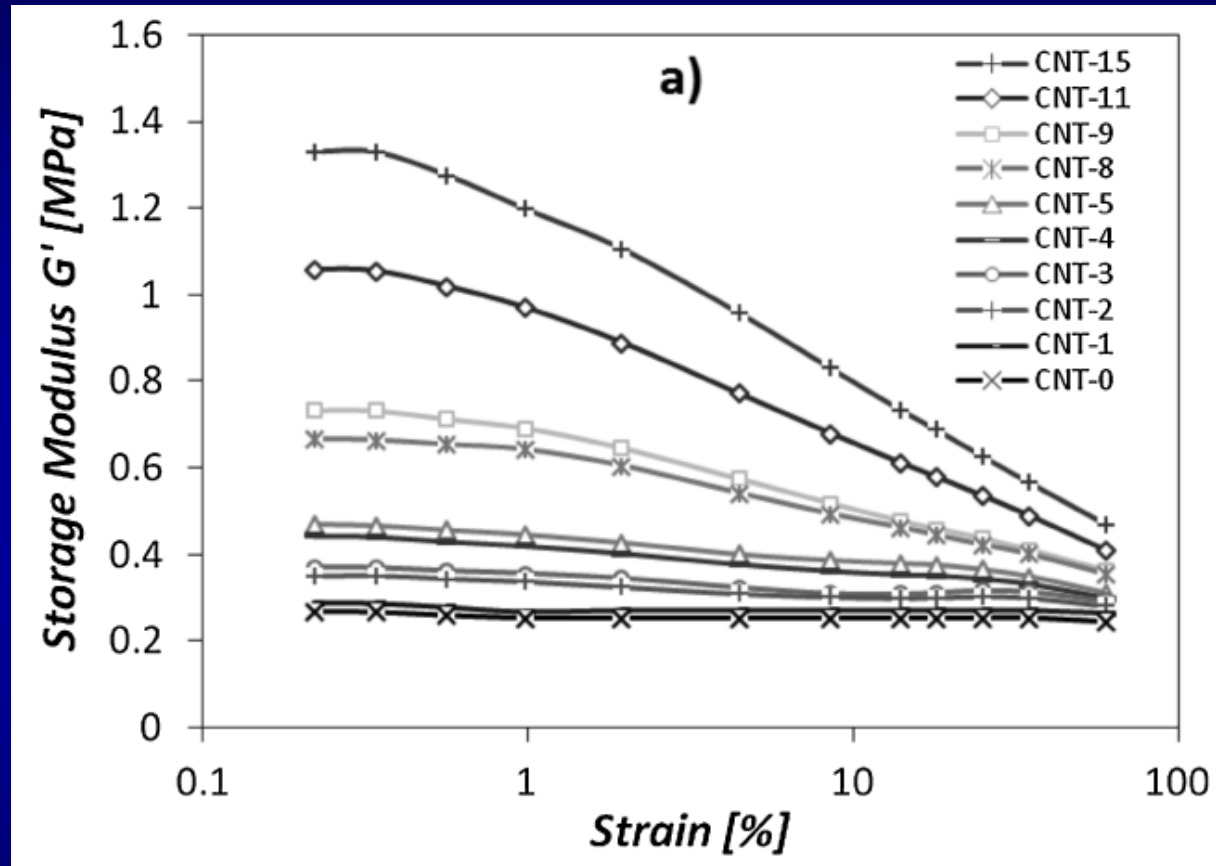


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Non linearity of dynamic mechanical behaviour



Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
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Hybrid filler systems based on CNT

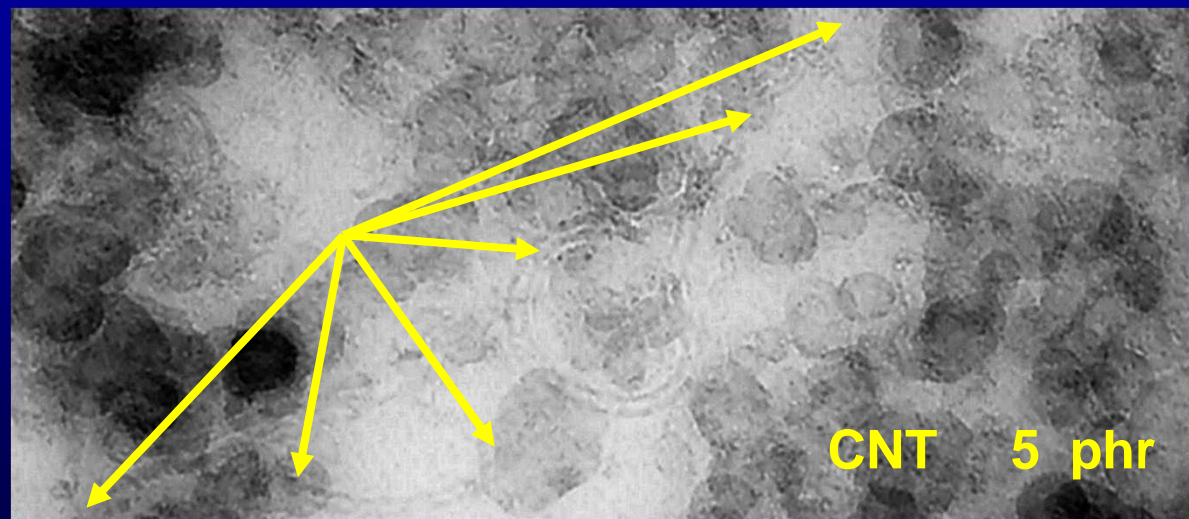
IR + CB + CNT nanocomposites - TEM micrographs

CNT	0	1.1	2.3	3.4	4.6	5.7	8	11.3
Other ingredients: ZnO 4 , Stearic acid 2 , Sulphur 2 , CBS 1 , Phtalic Anhydride 1								

IR = 100 CB = 60

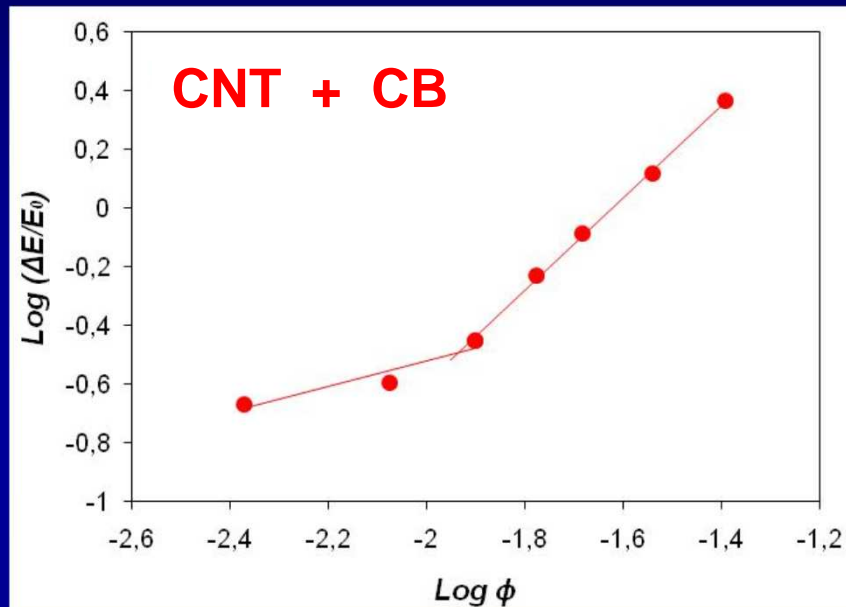


👉 High affinity of CNT for Carbon Black

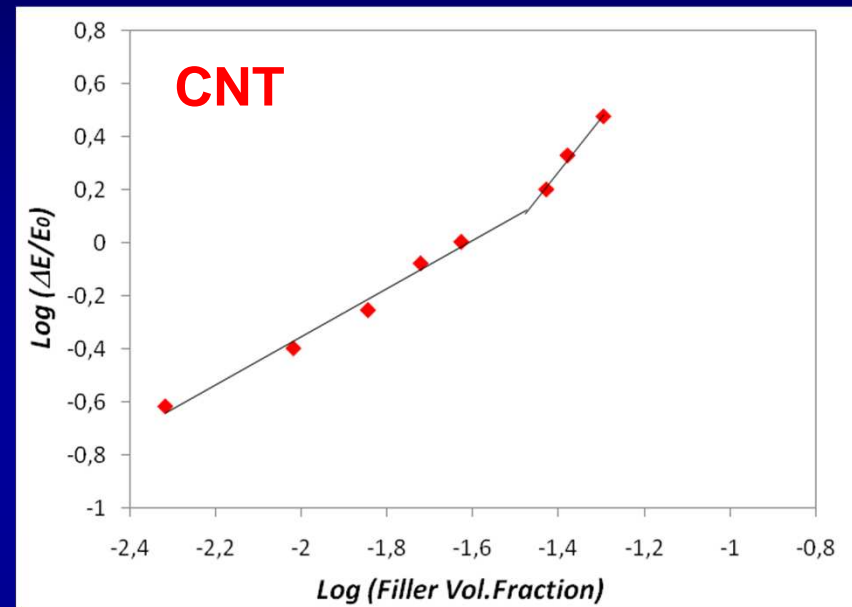


IR + CB + CNT nanocomposites - Filler network

Filler percolation threshold



$$\text{phr} = 2.8$$

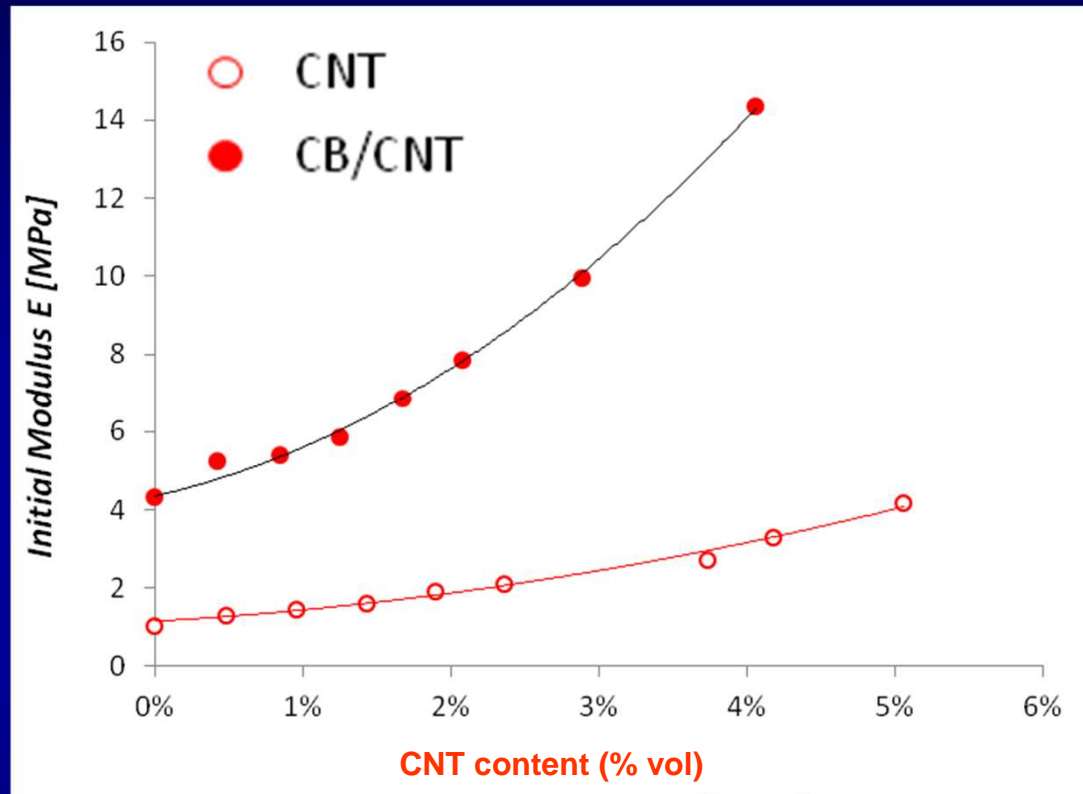


$$\text{phr} = 7.2$$

G. Huber, T. A. Vilgis,
Kaut Gummi Kunstst. 1999, 52(2), 102-7

Galimberti M., Coombs M., Riccio P., Ricco` T., Passera S., Pandini S., Conzatti L., Ravasio A., Tritto I.
Macromol. Mater. Eng. 2012, 298(2), 241-251

IR + CB + CNT nanocomposites - Initial modulus



Galimberti M., Coombs M., Cipolletti V., Riccò T., Agnelli S., Pandini S., KGK 2013 in press

Interactions between CB and nano-fillers

First approach:

Prediction of E modulus from simple additive model

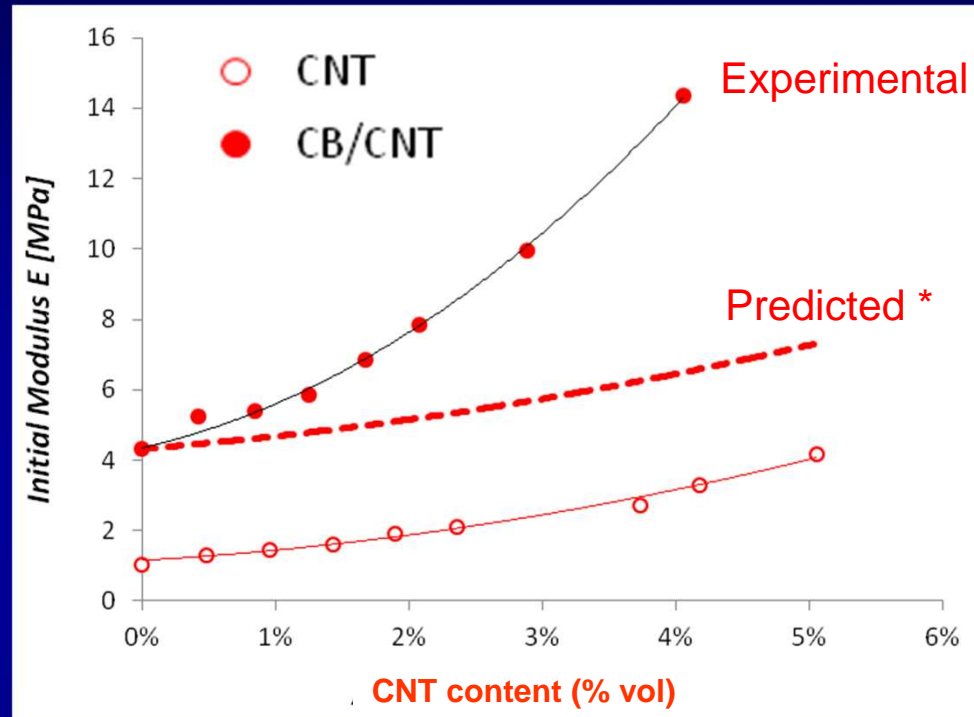


$$E (\text{CB} + \text{nanofiller}) = E (\text{CB}) + E (\text{nanofiller}) - E (\text{IR})$$

For interacting mixtures
there should be an interactive term

S.S. Sternstein, G. Ramorino, B. Jang, Ai-Jun Zhu. *RCT* vol. 78 (2), 258-270, (2005)

IR + CB + CNT nanocomposites



$$* E (CB+CNT) = E (CB) + E (CNT) - E (IR)$$

Galimberti M., Coombs M., Cipolletti V., Riccò T., Agnelli S., Pandini S., KGK 2013 in press

Interactions between CB and nano-fillers

$$E (\text{CB} + \text{nanofiller}) = E (\text{CB}) + E (\text{nanofiller}) - E (\text{IR}) + \Delta E$$

Interactive term



Caveat!

- ☞ Δ is due to non linearity of reinforcement
- ☞ Different relative amount of fillers

S.S. Sternstein, G. Ramorino, B. Jang, Ai-Jun Zhu. *RCT* vol. 78 (2), 258-270, (2005)

Composites based on CB and CNT

IR = 100



CB	0	2.50	5.00	10.00	15.00	30.0
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CNT	0	2.50	5.00	10.00	20.00
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CB	0	1.25	2.50	5.00	10.00
CNT	0	1.25	2.50	5.00	10.00

Recipes in phr, Fillers with the same volume fraction

Composites crosslinked with dicumyl peroxide: 1.40 phr

Interactions between CB and nano-fillers

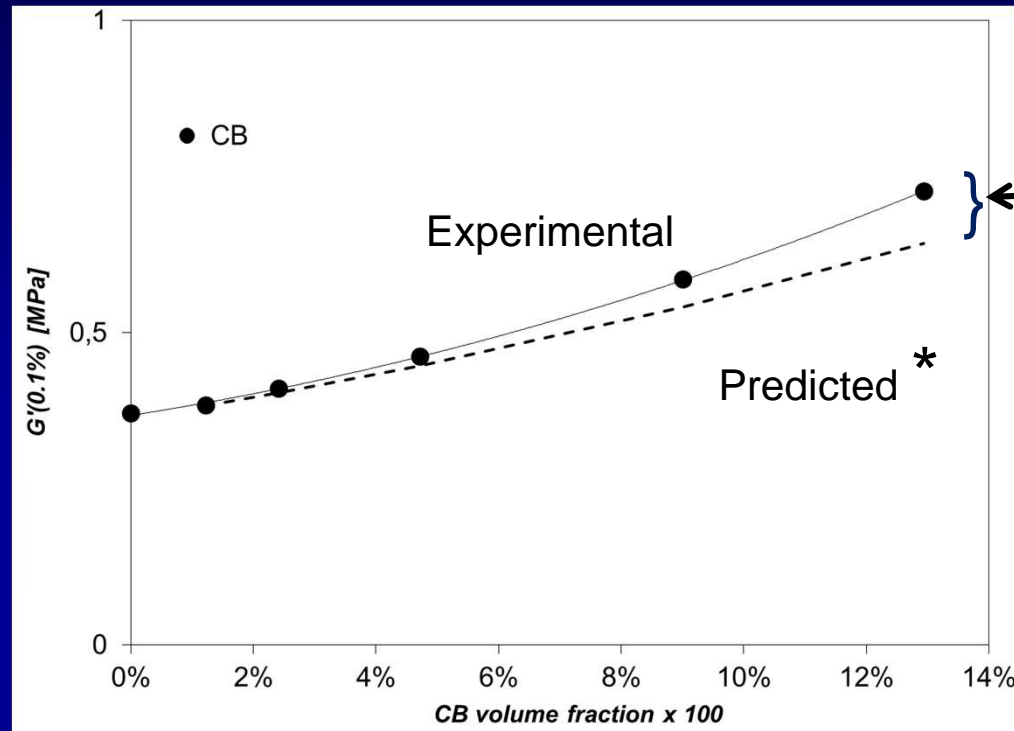
$$G'(\text{CB} + \text{filler}) = G'(\text{CB}) + G'(\text{filler}) - G'(\text{IR}) + \Delta G'$$

Interactive term



$$\Delta G' = G'(\text{CB} + \text{filler}) - G'(\text{CB}) - G'(\text{filler}) + G'(\text{IR})$$

Composites based on CB

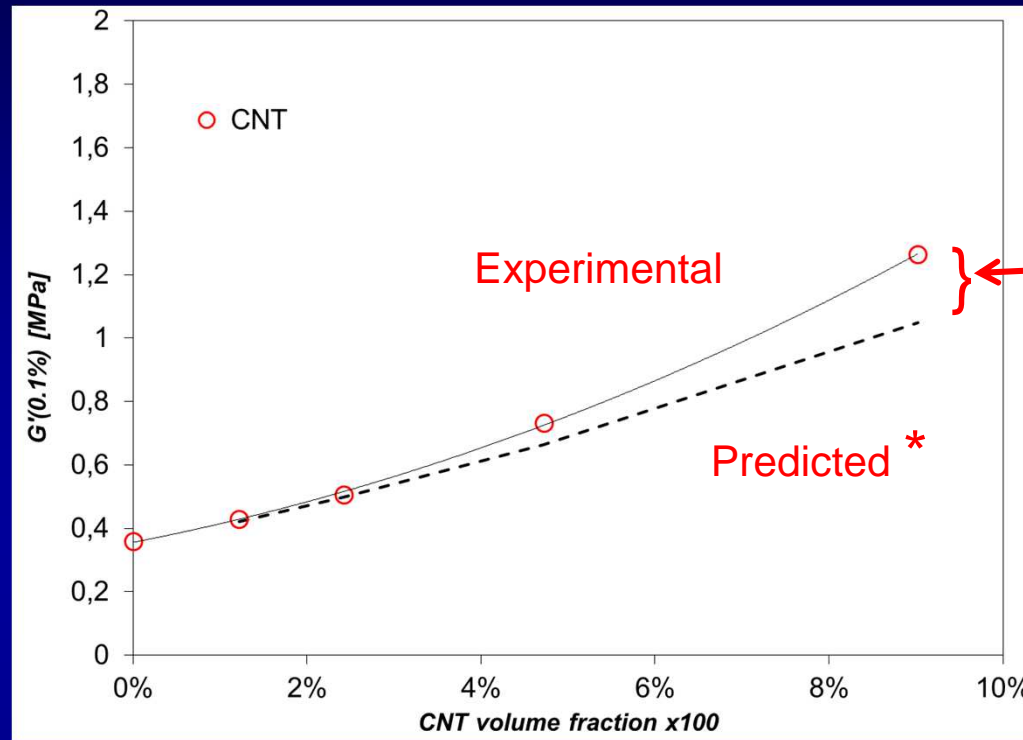


Interactive term $\Delta G'$

For a given volume fraction χ_i

$$* [G'_{\text{predicted}}(\text{CB} + \text{CB})]_{\chi_i} = G'(\text{CB})_{\chi_i/2} + G'(\text{CB})_{\chi_i/2} - G'(\text{IR})$$

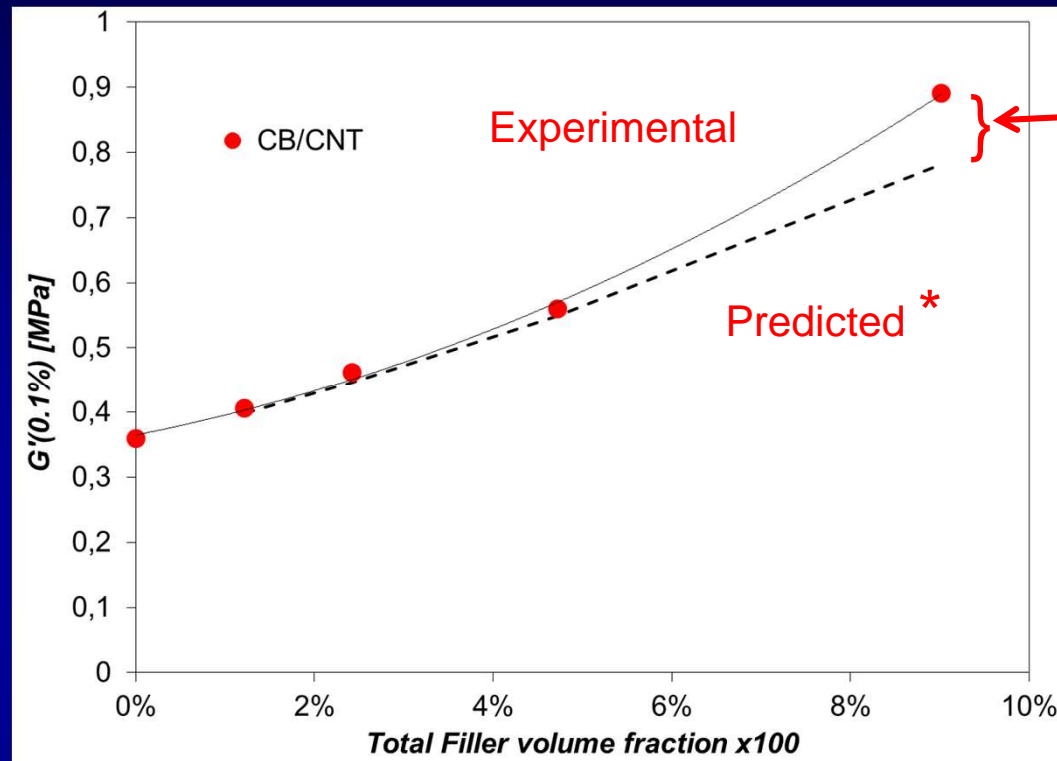
Composites based on CNT



For a given volume fraction χ_i

*
$$[G'_{\text{predicted}}(\text{CNT} + \text{CNT})]_{\chi_i} = G'(\text{CNT})_{\chi_i/2} + G'(\text{CNT})_{\chi_i/2} - G'(\text{IR})$$

Composites based on CB and CNT

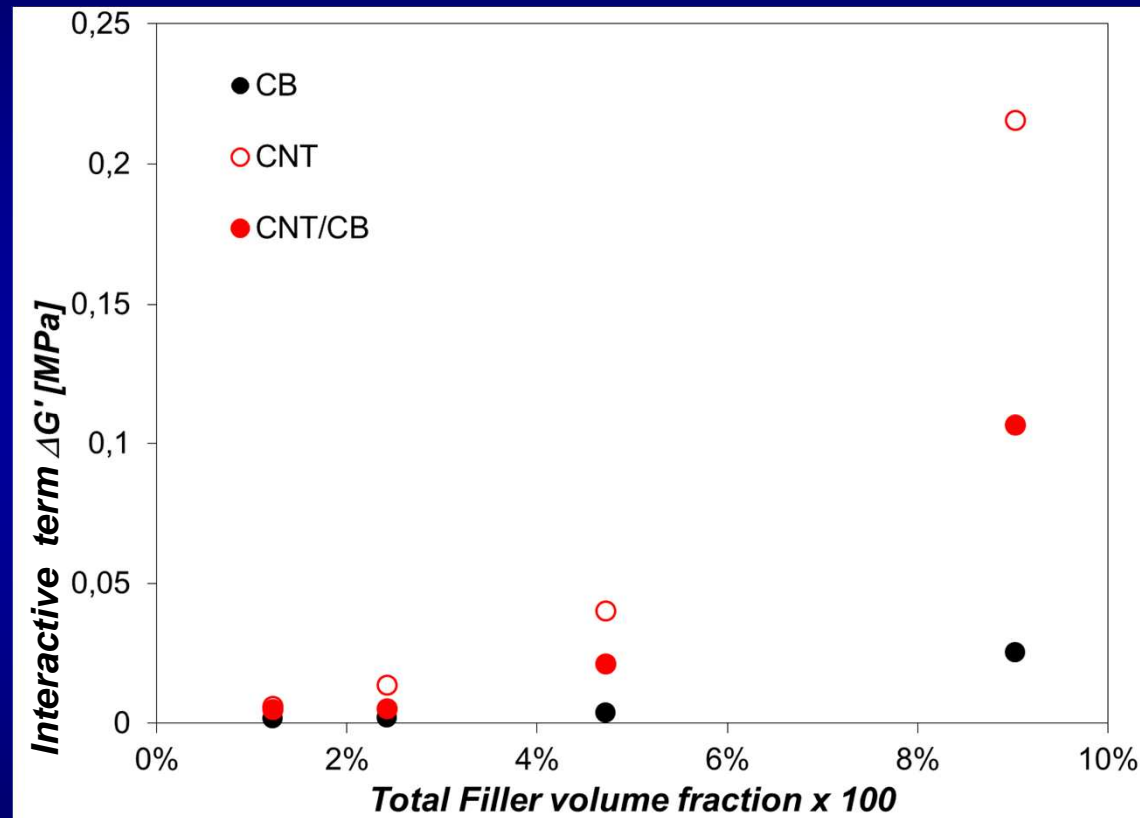


For a given volume fraction χ_i

*
$$[G'_{\text{predicted}}(\text{CB} + \text{CNT})]_{\chi_i} = G'(\text{CB}) \chi_i / 2 + G'(\text{CNT}) \chi_i / 2 - G'(\text{IR})$$

Composites based on CB and CNT

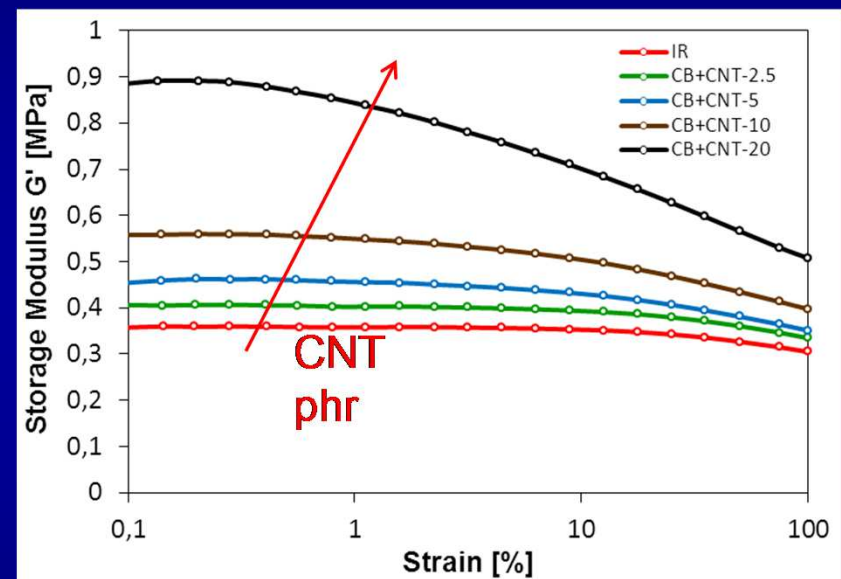
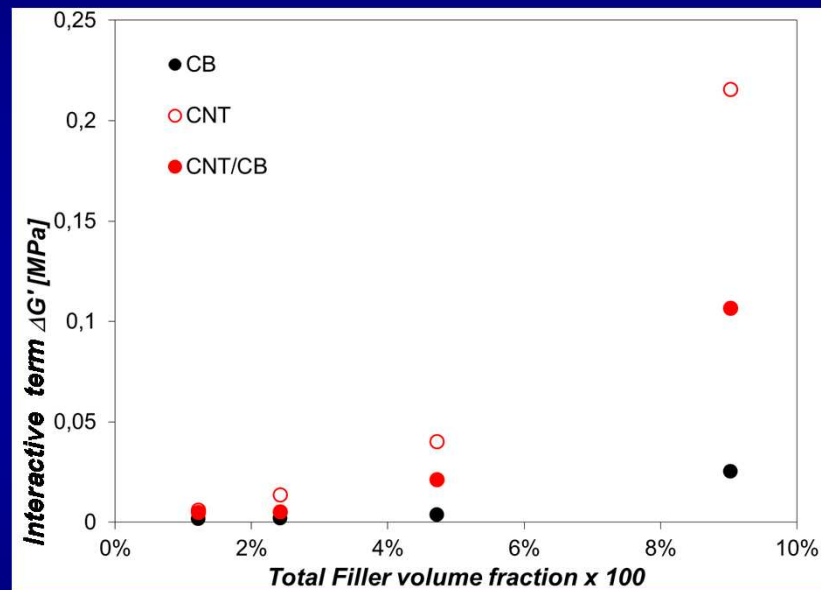
Interactive term $\Delta G'$ vs total filler volume fraction



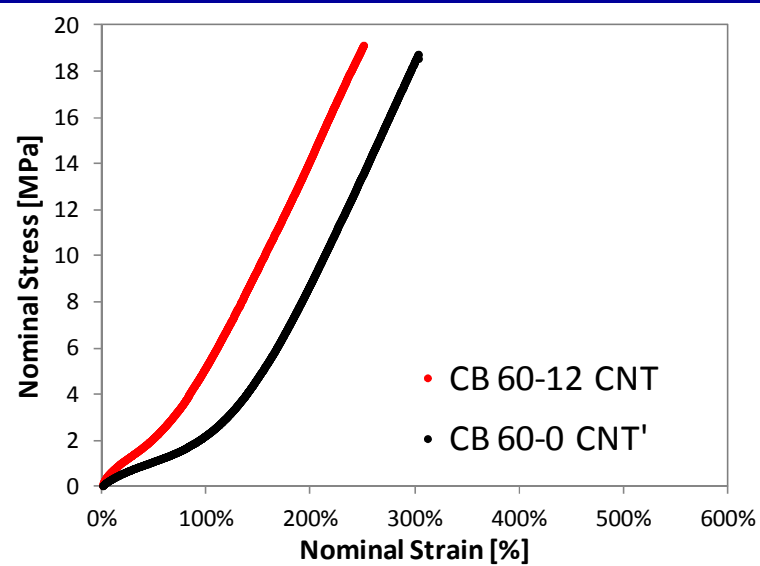
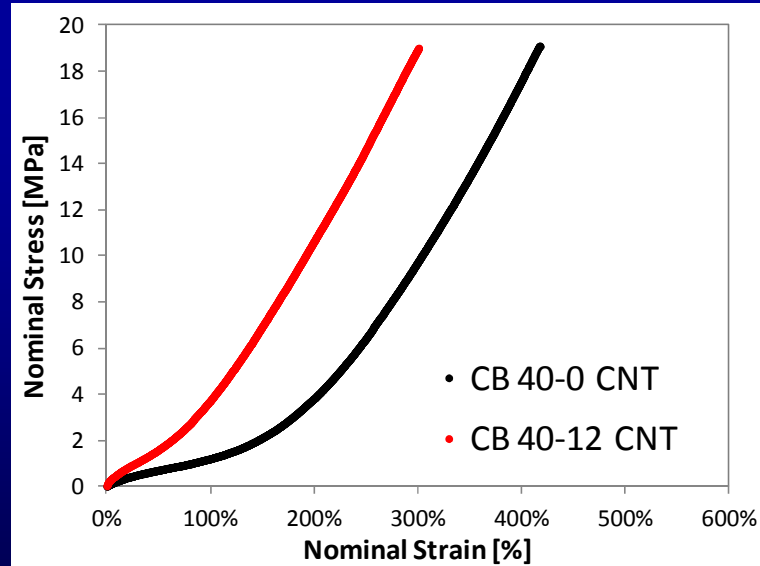
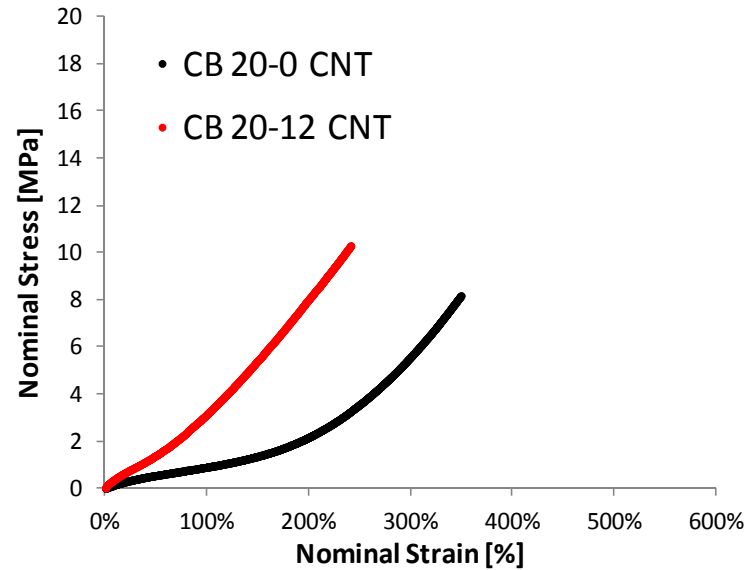
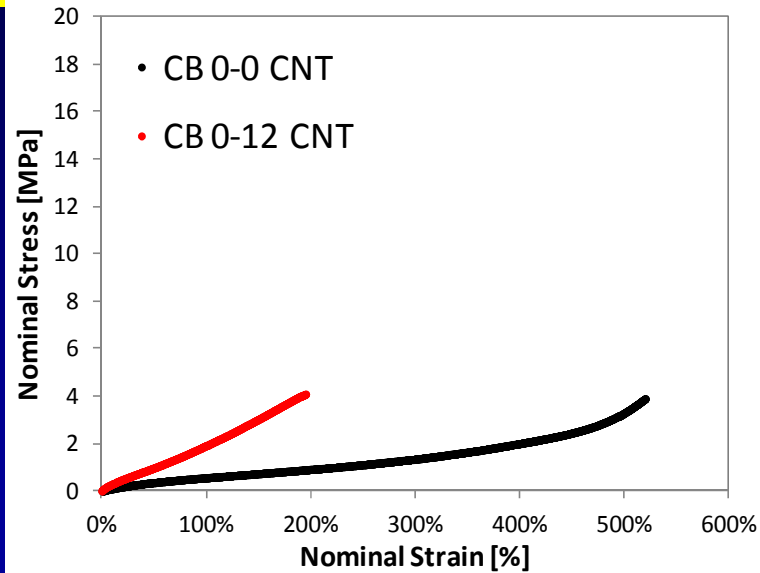
M. Galimberti, M. Coombs, V. Cipolletti, T. Riccò, S. Agnelli, S. Pandini,
Presentation at "KHK 10th Fall Rubber Colloquium, Hannover (D), November, 7th - 9th 2012"

Non linearity of dynamic mechanical behaviour

Shear storage modulus vs strain amplitude



Hybrid filler systems: CNT + CB – Stress strain curves



M. Galimberti et al Presented at 181th Technical Meeting of the Rubber Division of ACS, San Antonio (TX) April 22-25, 2012

Conclusions: CNT

- ☞ Enhance
 - electrical conductivity
 - thermal conductivity
 - mechanical properties
 - vulcanization efficiency
- ☞ Can be evenly distributed and dispersed through “drop in” processing technologies
- ☞ Can be used in a much lower amount with respect to traditional fillers
- ☞ Establish hybrid filler networks